TAB # 2

Appendices A - F1

This section of the ECA document contains the Appendices to the ECA. Additional changes and corrections to the ECA document were identified after completion of the Public Review Process. EPA set in place a process whereby the needed changes(s) were made using strike-out with hand written correction(s) on each page (i.e., replacement page) of the ECA where such changes were needed. Each signatory was asked to acknowledge their concurrence by initialing and dating every change on each ECA replacement page. To maintain continuity within the document, TAB #2 contains replacement pages initialed by EPA only. The initialed replacement pages from each Signatory Company are included under TABs #4 - #7 of this document.

APPENDIX A.1

LIST OF CHEMICAL COMPONENTS OF THE COMPOSITES¹

The following table lists the seventeen (17) commercial fluoropolymer chemicals (made using ammonium perfluoroctanoate (APFO)) that are the subject to this ECA.

The identities of the fluoropolymers (made using APFO) that are components of the composites that are subject to this ECA were provided to EPA as support documentation of the Companies' LOI commitments. Some of this documentation, including certain aspects related to the identity of the test substance as described in Part II of this ECA and the table below, contains Confidential Business Information (CBI). In such instances EPA creates a comprehensive database for evaluation and comparison, and, when possible, provides a public version sanitized of CBI.

Subsequent analysis of the list of fluoropolymers received by EPA supported the conclusion that the individual chemicals listed below are representative of all known commercial fluoropolymer chemicals and the basic chemistries are represented by the four composite test substances that are subject to testing under this ECA (i.e., dry melt fluoropolymer resin, dry non-melt PTFE homopolymer resin/gum, dry non-melt fluoroelastomer resin/gum, aqueous fluoropolymer dispersions) (see ECA Appendix A.2 and A.3). The fluoropolymer structure is predominantly -(CF2)x- which is a potential source of PFOA. For all fluoropolymer products used in commerce, the -(CF2)- moiety is common to all polymers and the composites to be tested under this ECA testing program (see Appendix A.2-A.4) are representative of the individual component and non-component fluorochemicals.

A.1-1

¹ There is a Public and CBI version of Appendix A.1 because one or more of the Companies have asserted that details describing their chemical(s) are considered by them to be entitled to treatment as TSCA confidential business information (CBI) (see Part XIV. D. of this ECA regarding confidentiality of information).

	FLUOROPOLYMERS SUBJECT TO THIS ECA				
No.	CAS#/DCN#/ or ACC# ²	Chemical Name			
1	CAS # 9002-84-0	Ethene, tetrafluoro-, homopolymer			
2	CAS # 25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene)			
3	CAS # 26655-00-5	Propane,1,1,1,2,2,3,3-heptafluoro-3-[(trifluoroethenyl0oxy]-, polymer with tetrafluoroethene			
4	CAS # 25190-89-0	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with 1,1-difluoroethene and tetrafluoroethene			
5	DCN # 63040000026	ETFE			
6	CAS #35560-16-8	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with ethene and tetrafluoroethene			
7	CAS #9011-17-0	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with 1,1-difluoroethene			
8	CAS #54675-89-7	1-Propene, polymer with 1,1-difluoroethene and tetrafluoroethene			
9	CAS #27029-05-6	1-Propene, polymer with tetrafluoroethene			
10	CAS #26425-79-6	Ethene, tetrafluoro-, polymer with trifluoro(trifluoroethoxy)ethene			
11	CAS #9010-75-7	Ethene, chlorotrifluoro-, polymer with 1,1-difluoroethene			
12	CAS #31784-04-0	Ethene, tetrafluoro-, polymer with trifluoro(pentafluoroethoxy)ethene			
13	DCN # 6304000018A	Polytetrafluoroethylene			
14	DCN # 6304000018B	Polytetrafluoroethylene			
15	DCN # 6304000018C	Fluoroelastomer			
16	DCN # 6301000018D	Fluoroelastomer			
17	ACC # 137678	Low Temperature Fluoroelastomer			

A.1-2

² EPA uses a variety of numerical identification systems for tracking chemicals. These include Chemical Abstract Service Registry numbers (CAS) (assigned to non-confidential listed chemicals), pre-manufacture notice (PMN) numbers (assigned by EPA when chemicals enter EPA's new chemical review process, document control numbers (DCN) (assigned by the Confidential Business Information Center for EPA tracking), and Accession (ACC) numbers (provided by EPA when a chemical identity requires protection as TSCA CBI). In addition, Polymer Exemption products will not have a TSCA Inventory ID number but may have a commercial trade identity.

Contains No Confidential Business Information

APPENDIX A.2

RATIONALE FOR SELECTING COMPOSITES TO BE TESTED

Review of Figure A.2-I demonsrates that fluoropolymers industry products can be divided into 3 broad categories as follows:

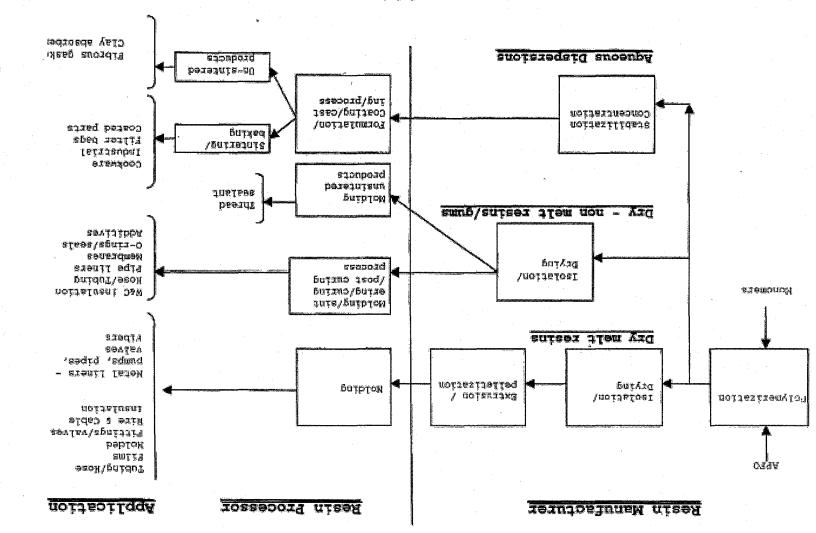
- Dry melt resins
- Dry non-melt resins and gums
- Aqueous dispersions

These three broad categories can in turn be divided into four representative classes as follows:

- Dry melt resins
 - 1. FEP, PFA, THV, ETFE, HTE
- Dry non-melt resins and gums
 - 2. Dry non-melt resins
 - 3. Fluoroelastomers (dry non-melt gums)
- Aqueous dispersions
 - 4. PTFE, FEP, PFA, THV

Composite samples of each of these four representative classes were selected as the test substance for this testing program in order to represent the entire range of fluoropolymers involved.

Figure A.2-1. Fluoropolymer Industry Overview



APPENDIX A.3 COMPOSITION OF COMPOSITES TO BE TESTED

The four composite test substances for this test program are presented below in Table A.3-I with the fluoropolymer types, CAS numbers, and associated monomers for these fluoropolymers. Each fluoropolymer used in each relevant test substance composite will have been made using APFO.

Table A.3-1. Test Substance Composites by Type

Test Substance	Fluoropolymer Type	•	Associated Monomers
Composite I -	PTPS	9002-84-0	Lee
Dry non-melt resin	Modified PIFE	26653-00-5	TFE, PPVE
Composite 2 -	EBP	25067-11-2	TEE, HEP
Dry melt resins	pta	26655-00-5 31784-04-0	TFE, PPVE TFE, PEVE
	THY	25190-89-0	TFS, HFP, VDE
	STEE	60250-05-5	TFE, E
•	HTE	35560-16-8	TPE, HFP, B
Composite 3 - Fluoroelastomers	Fluoroelastomer Copolymers	9011-17-0	VOP, HFP
	Fluoroelastomer Terpolymers	25190-89 - 0	TPE, RFP, VDF
	Base resistant elastomers	27029-05-6	PFE, VOF, P TFE, P
•		26425-79-6	Tee, pave
	CTFE elastomers	9010-75-7	CTEE, VED
	Low temperature elastomers		TFE, VOF
omposite 4 - queous	PTES	9002-84-0	re
ispersions	rep	25067-11-2	CFE, HFP
		26655-00-5	FFE, PRVE
· · · · · ·			IFE, HEP, VDF

W8 10/6/04

Confidential business information (CBI) regarding the chemical identity of low temperature elastomers has been submitted to EPA under separate cover.

Contains	No	Confid	lential	Business	Inform	nation
Contains	110	CUILLIU	LUILUIGI	Dubiness		uauvi

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APPENDIX A.4 PREPARATION OF COMPOSITES TO BE TESTED

4.1 Approach

A composite mixture of representative fluoropolymers, as solids, will be prepared for each of the four test substance composites.

The polymer samples will be first quality product polymer, substantially free of inorganic constituents. Each sample will be from a representative grade for each applicable fluoropolymer type from each applicable company.

A hypothetical example for Composite Z in Table A.4-1 below shows how the composites will be assembled. In this example with 4 types across 4 companies, there are 11 x's. Hence, composite Z would be made up of 11 equal proportions of the materials indicated with an x.

Table A.4-1. Example for Compositing Across Companies & Types

Test Substance	Fluoropolymer Type	Coupeny A	Сопр апу В	C	Company D
Composite Z	Type 1		X	X	X
	Type 2	X	Х	X	x
	Type 3			X	
	Type 4	X	X	×	

4.2 Preparation

Representative samples of each component from each applicable company for each composite will be sent to the compositing facility(ies) in packaging customarily used for product sample packaging or in polyethylene, polypropylene, or glass containers.

Each composite will be prepared under conditions designed to prevent cross-contamination and designed to assure solids temperatures less than or equal to 60 °C.

Following preparation of each composite, the composite will be placed in a polyethylene, polypropylene, or glass container.

4.2.1 Composite 1

Dry non-melt resins are available in powder form. Equal weights of the powder form of each of the two types of components (following the approach in the example for Composite Z in Section 4.1 above) will be mixed together in dry form to yield Composite 1.

4.2.2 Composite 2

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FEP, PFA ETFE

EEP, PEA, THV, ETEE, and HTE dry melt resins are available in powder form. Equal weights of the powder form of each component (following the approach in the example for Composite Z in Section 4.1 above) will be mixed together in dry form to yield Composite 2.

4.2.3 Composite 3

Fluoroelastomers are available in slab, lump, or sheet form. Composite 3 will be prepared following one of the following approaches:

a) Equal weights of each component (following the approach in example for Composite Z in Section 4.1) will be mixed on a rubber mill to produce a homogenous slab of preset thickness to yield Composite 3.

Or

b) Each component of Composite 3 will be cyrogenically cooled (to make the elastomers brittle) and size-reduced (e.g., ground) to produce powder. Equal weights of the powder form of each component (following the approach in the example for Composite Z in Section 4.1) will be mixed together in dry form to yield Composite 3.

4.2.4 Composite 4

Aqueous dispersions of PTFE, FEP, PFA, and THV are available as dispersions containing 20 to 60% fluoropolymer solids by weight. Composite 4 will be prepared following one of the following approaches:

a) Equal weights (on a dry solids basis) of each component in aqueous dispersion form (following the approach in example for Composite Z in Section 4.1) will be mixed together in liquid form. Solids will be separated from the resulting liquid composite to yield low water content (i.e., drip free) fine solids.

Or

b) Solids will be separated from liquid for each component of Composite 4 to yield low water content (i.e., drip free) fine solids for each component. Equal weights of the solids form of each component (following the approach in the example for Composite Z in Section 4.1) will be mixed together to yield Composite 4.

4.3 Verification

In order to assure that composite samples in this testing program have been made up of clearly identified materials, the preparation of the composites will include formal Chain of Custody procedures. A chain of custody form will be included with each component material going into the composite to show the identity of the component material and each transfer of custody from its point of origination to preparation of the composite.

Once prepared, each composite will be accompanied by a new chain of custody until it reaches the incineration testing facility.

For documentation, the facility preparing a given composite will generate a report to be submitted to EPA with the final report for Phase II incineration testing.

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APPENDIX B.1

GUIDELINE FOR THERMOGRAVIMETRIC ANALYSIS

As described in Appendix C.2.3, thermogravimetric analysis will be conducted as part of this testing program. An available standard method (ASTM E 1868-02) has been adapted for conducting this thermogravimetric analysis to determine the temperature range required for gasification. Therefore, ASTM E 1868-02 "Standard Test Method for Loss-On-Drying by Thermogravimetry" will be used as the guideline for conducting the analysis described in Appendix C.2.3 with the following modifications for this testing program:

Section	Modification
2.1	• Standard practices at the University of Dayton Research Institute (UDRI) may be used as references throughout the standard in place of the ASTM standards noted in this section as they are not needed for this testing program.
4.1	The loss-on-drying value specified in the second through fifth sentences of this section will not be recorded as this value is not needed for this testing program.
7.1.3	• The programming rate of the furnace will be set at 10 to 25°C/min, rather than 5°C/min. Pursuant to section 11.6, the temperature program rate will be documented in the report.
	 The isothermal temperature within the range of 25 to 1000°C will be maintained ±3°C, rather than ±2°C.
7.1.4	 The specimen atmosphere control system will be capable of supplying dry air in addition to "inert dry gas (usually purified grade nitrogen)".
7.1.7	• The temperature program rate will be set at 10 to 25°C/min, rather than 5°C/min. Pursuant to section 11.6, the temperature program rate will be documented in the report.
	• The temperature program rate will be controlled to within the range of ±3°C/min, rather than ±0.1°C/min.
	 Within the range of 25 to 1000°C, the isothermal temperature will be maintained within ±3°C, rather than ±2°C.
11.4	• The mass of the test specimen noted in the first sentence of this section will be 0.005 to 5 mg, rather than 10±1 mg (i.e., 9 to 11 mg).

11.6	• The test specimen heating rate will be set at 10 to 25°C/min, rather than 5°C/min noted in the first sentence of this section. Pursuant to section 11.6, the temperature program rate will be documented in the report.
11.9	• Termination criteria will follow Test Method A as outlined in section 11.10.1.
11.10.1	• The "fixed period of test time" mentioned in this section will be set at 5 min.
11.10.1.1	• Loss-on-drying values will not be recorded.
12.1	• The loss-on-drying value will not be calculated.
13.1.1	 The "identification and description of the material being tested" will be consistent with the information known to the analyst.
13.1.5	• The loss-on-drying value will not be included in the report.
14.2	• This section is not applicable because the Test Method A termination criteria will be used.

16 Reference

ASTM E 1868-02 "Standard Test Method for Loss-On-Drying by Thermogravimetry", ASTM International. For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For Annual Book of ASTM Standards volume information, refer to the standard's Document Summary page on the ASTM website.

APENDIX C.1 PFOA TRANSPORT TESTING

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C.1.1 Significance

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Testing will be performed to verify that potential PFOA emissions from the combustion testing described in Appendix C.2 can be quantitatively transported from the high temperature reactor into the exhaust gas sampling apparatus (aqueous solution bubblers).

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Acceptable PFOA transport will be demonstrated if the transport efficiency (as computed in one or more of the formulas below) is greater than or equal to 70%.

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C.1.2 Experimental Plan

17: 18

C.1.2.1 Base Plan

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Transport of PFOA across the laboratory-scale thermal reactor system described in Appendix C.2.4 and into the exhaust gas bubblers described in Appendix D.1 will be quantitatively determined as an indication of transport from the high temperature reactor into the bubblers.

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A PFOA standard of known purity greater than or equal to 97% will be gasified at 150 to 300 °C (based on thermogravimetric analysis of PFOA) with transfer line and reactor temperatures 0 to 150 °C higher than the gasification temperature. With the exception of temperature as noted above, the target operating conditions for the high temperature reactor of the thermal reactor system will be consistent with the conditions presented in Table C.2-1 in Appendix C.2.4.

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Three replicate transport efficiency test runs will be conducted. A minimum of one blank run will be conducted prior to each transport efficiency test run.

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The sample size of the PFOA standard to be gasified will be The reactor exhaust gas will be collected less than 5 mg. into bubbler aqueous solution as described in Appendix D.1 (including an HPLC water rinse of the flexible tubing [used to connect the thermal reactor system and the bubbler assembly] into the aqueous solution composite), which will be analyzed for PFOA as described in Appendix D.2. order to provide a second way of demonstrating quantitative

04-22-04 transport, this aqueous solution composite will also be analyzed for total fluorine as described in Appendix D.3. (Testing for total fluorine is included due to possibility 3 of thermal degradation of PFOA under transport test 4 Therefore, for this transport testing the 5 conditions.) amount of PFOA fed to the thermal reactor system will be sufficiently high to assure that the total fluorine input 7 to the thermal reactor system will be greater than 140% of 8 the mass corresponding to the limit of quantitation (LOQ) 9 for total fluorine in the aqueous solution composite. 10 LOO for total fluorine in aqueous solution is much higher 11 than the LOQ for PFOA in aqueous solution.) 12 13 The amount of PFOA and total fluorine in the thermal 14 reactor system exhaust gas will be determined via analysis 15 of the aqueous solution composite as noted above. 16 17 The amount of PFOA fed to the thermal reactor system will 18 be known based on measurement prior to gasification and 19 will be verified by weighing the pyroprobe insert cartridge 20 before and after each test run. The amount of fluorine 21 input to the system will be calculated from the amount of 22 PFOA fed, the known purity of the PFOA, and the known 23 fluorine fraction of the PFOA standard. 24 25 PFOA transport efficiency (TE) as a percentage will be computed as follows: 27 28

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45 46 47 % PFOA TE = mass of PFOA in aqueous solution composite * 100 (1)mass of PFOA fed to thermal reactor system

Total fluorine (TF) transport efficiency as a percentage will be computed as follows:

% Total F TE = mass of total F in aqueous solution composite * 100 mass of total F fed to thermal reactor system

C.1.2.2 Contingent Testing

If the transport efficiencies for both PFOA (equation 1) and total fluorine (equation 2) are less than 70%, then additional work will be performed. This additional work will be performed in a step-wise fashion to determine if consideration of one or more of the following procedural revisions enables achievement of 70% transport efficiency as follows:

```
The flexible tubing between the thermal reactor
     Step 1.
               system and the bubbler assembly from the experiment
               described in Section C.1.2.1 would be
 3
               quantitatively rinsed with methanol. This methanol
 4
               rinsate would be analyzed for PFOA (as described in
 5
               Appendix D.2) and/or for total fluorine (as
 6
               described in Appendix D.3).
                                                Revised transport
 7
               efficiency (TE) as a percentage for PFOA (equation
 8
               3) and/or total fluorine (equation 4) would be
 9
               computed by including the mass of analyte in the
10
               methanol rinse in the numerator as follows:
11
12
13
                           mass<sub>PFOA</sub> out
               % PFOA TE = ---- * 100
                                                                        (3)
14
15
                           mass<sub>PFOA</sub> in
16
                           where mass_{PFOA} out =
                                               mass of PFOA in bubbler
17
18
                                               aqueous solution composite
                                               + mass of PFOA in methanol
19
20
21
                                              mass of PFOA fed to thermal
                           and mass<sub>PFOA</sub> in =
22
                                              reactor system
23
24
25
                             mass<sub>total F</sub> out
               % Total F TE = ----- * 100
26
                                                                       (4)
27
                             mass<sub>total F</sub> in
28
                             where mass_{total \ F} out = mass \ of \ total \ F \ in
29
                                                   bubbler aqueous
30
                                                   solution composite
31
                                                   + mass of total F in
32
33
                                                   methanol rinse
34
35
                                                   calculated mass of
                              and mass<sub>total F</sub> in =
                                                   total F in PFOA fed to
36
                                                   thermal reactor system
37
38
                            The experiment described in Section
39
     Step 2 (if necessary)
                            C.1.2.1 would be repeated with
40
                            reagent(s) (e.g. NaOH) added to the
41
                            bubbler aqueous solution to determine
42
                            if reagent addition enhances analyte
43
                            absorption, thereby improving transport
44
                            efficiency. Transport efficiency would
45
                            be calculated using equation (1) and/or
46
47
                            (2) above. The impact of reagent
                            addition on LOQ for PFOA analysis
48
                            described in Appendix D.2 would be
49
                            determined.
50
51
```

. 2 Following completion of PFOA transport testing as described 3 in this appendix and prior to beginning incineration 4 testing described in Appendix C.2, a letter report will be 5 submitted to EPA with the transport efficiency result(s) and indication of what contingent testing, if any, was 7 8 performed. 9 If Appendix C.2 incineration testing is performed, the 10 detailed results of Appendix C.1 transport testing will be 11 12 included in the test report for Appendix C.2 incineration testing described in Appendix C.2.5. If Appendix C.2 13 incineration testing is not performed, the detailed results 14 of Appendix C.1 transport testing will be provided in a 15

test report for Appendix C.1 transport testing.

C.1.3 Reporting of Results

APPENDIX C.2 INCINERATION TESTING

C.2.1 ELEMENTAL ANALYSIS

C.2.1.1 Introduction

Elemental analysis as described in Section C.2.1 will be performed for each test substance composite to aid in preparation for combustion testing described in Section C.2.4.

As Kissa (1998) points out, technique strongly affects analytical results for fluorinated organic compounds such as fluorinated surfactants and fluorinated polymers due to the carbon-fluorine bond:

Fluorine in organic compounds is usually determined by converting organic fluorine to an inorganic fluoride. Various combustion methods are routinely used for this purpose. However, the carbon-fluorine bond is exceptionally strong, and extremely vigorous conditions are needed for a quantitative mineralization. Conventional combustion conditions used for the determination of carbon and hydrogen in nonfluorinated organic compounds are not adequate for a quantitative analysis of fluorinated surfactants.

Therefore, total fluorine analysis will be performed using "extremely vigorous conditions" as described in Section C.2.1.2, and the commercially available conventional technique used for empirical determination of carbon and hydrogen content (described in Section C.2.1.3) will provide estimated values.

C.2.1.2 Total Fluorine

Each test substance composite will be characterized via analysis of total fluorine content.

Based on manufacturing process knowledge, the levels of total fluorine in the components of test substance composites are orders of magnitude higher than the potential trace level of inorganic fluoride in these materials. Therefore, for this test program, the total

47 organic fluorine value for each test substance composite

will be considered to be the same as the total fluorine value.

Total fluorine content will be measured via the Wickbold Torch method; see Appendix D.3.

C.2.1.3 Carbon and Hydrogen

In order to provide information for stoichiometric calculations in Section C.2.2, the carbon and hydrogen content of each test substance composite is needed. Based on manufacturing process knowledge of the polymers in this program, levels of sulfur, and nitrogen are expected to be less than 0.1% and to thereby have negligible effect on stoichiometric calculations.

C.2.1.3.1 Theoretical Determination

Where the elemental composition of a test substance composite is known from the identity of the components in a given composite, the carbon and hydrogen content of the test substance composite can be calculated.

For example, where each of the components of a test substance composite are polytetrafluoroethylene (PTFE), the carbon and hydrogen can be determined knowing the molecular formula for PTFE is $(C_2F_4)_n$ as follows:

	number	atomic weight	weight %
carbon (C)	2	12	24
hydrogen (H)	0	1	0
fluorine (F)	4	19	76
total		and the second	100

C.2.1.3.2 Empirical Determination

Where compositional information on carbon and hydrogen content is not known from the identity of the components in a given composite, each such test substance composite will be analyzed for carbon and hydrogen.

 As noted in Section C.2.1.1, empirical determination of carbon in test substance composites via commercially available conventional techniques is expected to underestimate the carbon content of the test substance composites due to the strength of the carbon-fluorine bond. Similarly, empirical determination of hydrogen in test

C.2-2

substance composites via commercially available conventional techniques is expected to overestimate the hydrogen content of the test substance composites.

4

The carbon content of the test substance composite can be 5 measured by determining the carbon dioxide (CO2) generated 6 7 by the oxidation of the sample. This oxidation may be accomplished by high temperature combustion, catalytic 8 combustion, or wet chemical oxidation. The CO2 is measured 9 directly by an infrared detector or a thermal conductivity 10 detector, via absorption into a suitable solution (e.g., 11 potassium hydroxide) and gravimetric determination, or by 12 conversion to methane for measurement via a flame 13 ionization detector. 14

15

The hydrogen content of the sample can be determined by 16 difference with knowledge of the fluorine content and 17 carbon content of the sample where the moisture content and 18 chlorine content of the sample are negligible or known. 19 Alternatively, the hydrogen content of the sample is 20 measured by determining the water generated by high 21 temperature combustion of the sample. Measurement of water 22 in the combustion gas for this analysis may be accomplished 23 by techniques such as use of an infrared detector or 24 absorption on a dessicant with gravimetric determination. 25 With empirical hydrogen determination, it is important to 26 correct for the water in the combustion gas attributable to 27 the moisture content in the sample to obtain the hydrogen 28 content of the sample; see Section C.2.1.4. 29

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Manufacturing process knowledge of the polymers will be used to review the elemental analysis results and to form the basis for interpreting non-detects. For example, if the hydrogen analytical result for a perfluorinated polymer is less than a quantitation limit of 0.1%, then the analytical result will be replaced with 0.

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C.2.1.4 Moisture

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Where preparation (as described in Appendix A.4) for a given test substance composite has involved dewatering, the moisture (or solids) content of each such test substance composite will be determined in order to provide a dry basis for calculations as needed.

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> 46 Moisture is determined by measuring the loss of weight of 47 the sample when heated under controlled conditions. A

representative sample is weighed and placed in a crucible (or dish) and evaporated to dryness in an air or nitrogen atmosphere at a defined temperature setpoint (e.g., 103 °C to 105 °C) in the range of 100 °C to 125 °C. The moisture value is calculated as the loss in weight (difference between the starting weight of sample and the final weight of sample) divided by the starting weight of sample. Similarly, a solids value can be calculated as the final weight of sample divided by the starting weight of sample.

C.2.2 COMBUSTION STOICHIOMETRY

Combustion stoichiometry calculations as described in Section C.2.2 will be performed to aid in preparation for combustion testing described in Section C.2.4

First, the weight percent values from Section C.2.1 are converted to molar quantities on a dry basis.

 Second, based on Chapter 3 of Combustion Fundamentals for Waste Incineration (American Society of Mechanical Engineers, 1974), the reaction products for these molar quantities are calculated assuming complete combustion with the following rules:

a) All carbon (C) in feed converts to carbon dioxide (CO₂) C + O₂ \rightarrow CO₂

b) All sulfur (S) in feed converts to sulfur dioxide (SO₂) S + O₂ \rightarrow SO₂

c) The halogens (Cl, F) in feed convert to hydrogen halides $\begin{array}{c} {\rm H_2} \,+\, {\rm Cl_2} \, \xrightarrow{} \, 2{\rm HCl} \\ {\rm H_2} \,+\, {\rm F_2} \, \xrightarrow{} \, 2{\rm HF} \end{array}$

d) Hydrogen (H) present in feed in excess of that required to yield products in item c) above will be converted to water $2H_2 + O_2 \rightarrow 2H_2O$

e) Nitrogen (N) from feed or air is emitted as molecular nitrogen $N_2 \, \xrightarrow{} \, N_2$

Third, with these rules, the balanced chemical reaction for combustion of a compound can be written.

For example, the resulting reaction equation for a hydrocarbon like methane (CH₄) is $CH_4 + 2 O_2 \rightarrow CO_2 + 2H_2O$

Note that the term feed in the preceding rules (a through e) includes both material being combusted and the fuel source of hydrogen such as methane or methanol.

Additionally, stoichiometric calculations as described above presume that the compounds undergoing combustion are essentially free of inorganic constituents.

These calculations provide the theoretical amount of oxygen needed for the overall combustion reaction for the feed based on the available information used in the .14 calculations. The initial estimate for the amount of oxygen to be used in combustion testing will be determined from this theoretical amount with adjustments for target oxygen level in thermal reactor system exhaust gas. actual amount of oxygen to be used in combustion testing will be based oxygen monitoring described in Section C.2.4.

These stoichiometric calculations will also be used as needed to initially estimate and adjust experimental conditions for combustion testing in Section C.2.4.

C.2.3 THERMOGRAVIMETRIC ANALYSIS

Thermogravimetric analysis (TGA) will be conducted to determine the temperature range required for gasification of each test substance composite. TGA will be conducted in flowing air from room temperature to 1000°C as described in Appendix B.1.

The TGA weight-loss profile for each test substance composite will be evaluated to determine the temperature at which the weight loss reaches a final asymptote across the temperature range investigated. This temperature corresponds to the point at which no further gasification (under test conditions) occurs for the material and will be considered the temperature for complete gasification of the material.

C.2.4 Combustion Testing

C.2.4.1 Test Objective

The objective of the testing program described in Appendix C.2 is to assess the potential for waste incineration of

each test substance composite to emit PFOA, based on quantitative determination of potential exhaust gas levels of PFOA from laboratory-scale combustion testing under conditions representative of typical municipal waste combustor operations in the U.S.

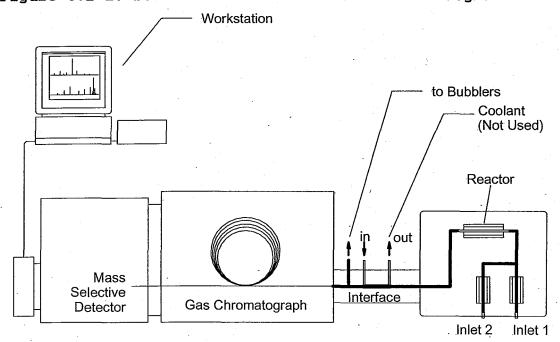
C.2.4.2 Experimental Apparatus

Combustion testing will make use of the Advanced Thermal Reactor System (ATRS) at the University of Dayton Research Institute (UDRI). The ATRS is a laboratory-scale, non-flame, batch-charged, continuous flow thermal reactor system. The use of this non-flame thermal reactor system gives a conservative representation of full-scale waste incineration prior to air pollution controls.

In the ATRS, the test sample is gasified and transported to a high temperature reactor. In the high temperature reactor, the sample vapors are subjected to controlled conditions for residence time and temperature. As described in Sections C.2.4.5 and C.2.4.6, combustion products will be monitored or collected for quantitative analysis.

A schematic of the ATRS as configured for this test program is shown in Figure C.2-1.

Figure C.2-1. Schematic of ATRS for this Test Program



The ATRS consists of a reactor assembly and in-line gas chromatograph/detector system connected via an interface. The reactor assembly consists of a thermally insulated enclosure housing the sample introduction, reactor, and transfer line systems.

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7 Sample introduction for solid materials (Inlet 1) employs a 8 pyroprobe, a device designed to gasify samples by heating 9 them at a fixed rate. The main gas flow will also be fed 10 via Inlet 1, and Inlet 2 will be used to feed supplemental 11 flow.

12

During combustion tests, the transfer line between the 13 pyroprobe and the reactor is heated and maintained above 14 200 °C. The reactor is housed within its own small tube 15 furnace and may be independently heated to as high as 1100 16 °C. (Actual conditions for this test program are presented 17 in Section C.2.4.3.) The transfer line from the reactor to 18 the interface is heat traced to greater than 200 °C to 19 prevent cool regions where reactor products could otherwise 20 be lost through condensation. 21

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The interface routes the combustion exhaust gas to the inline gas chromatograph (GC) and mass selective detector (MSD) or to sample collection for off-line analysis. For combustion testing in this test program, the interface will also be maintained above 200 °C. Exhaust gas monitoring for this program is described in Section C.2.4.5.

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C.2.4.3 Combustion Test Experimental Conditions

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Each test substance composite will be subjected to laboratory-scale incineration using the experimental apparatus described in Section C.2.4.2.

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C.2.4.3.1 Combustion Air

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38 Synthetic air (mixture of 21% oxygen and 79% nitrogen) will 39 be used in place of compressed air to prevent potential 40 interference in the experimental system due to background 41 levels of CO₂ in compressed air.

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C.2.4.3.2 Fuel

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Methanol will be used, as needed, as a supplemental fuel to ensure the presence of sufficient hydrogen to convert

fluorine to hydrogen fluoride (HF) and chlorine to hydrogen 2 chloride (HCl).

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As noted in Municipal Solid Waste in the United States: 4 2000 Facts and Figures (EPA, 2002), paper and paper products (made from wood) make up the largest component of municipal solid waste (MSW). The sum of paper and paper products with wood in MSW makes up over 30% of MSW.

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During the 19th century, methanol was produced from wood and was known as wood alcohol. Therefore, methanol can be used in this experimental program as a surrogate for the paper and wood fraction of MSW.

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C.2.4.3.3 Operating Conditions

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The target operating conditions for the high temperature reactor during the combustion tests for each test substance composite identified in Appendix A.3 are presented in Table C.2-1.

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TABLE C.2-1. COMBUSTION TEST TARGET OPERATING CONDITIONS

Temperature	1000 °C	
Residence Time	2 se	C
O ₂ concentration in exhaust gas	10%	
H ₂ O concentration in exhaust gas	15%	
Number of replicate runs	3	

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These conditions are conservatively representative of typical furnace operating conditions of municipal waste combustors (MWCs) and of typical secondary chamber operating temperatures for medical waste incinerators in the U.S. See Appendix D.4 for supporting information.

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Temperature and residence time values in Table C.2-2 will be fixed setpoints for these experiments. The temperature of the high temperature reactor will be controlled within +10 °C to assure isothermal operation.

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The amount of each test substance composite fed to the ATRS in this testing program will be a measured amount less than 5 mg. The actual amount fed, gasification rate (determined from TGA), air supply, and fuel supply will be adjusted to assure that the oxygen level in the exhaust will be greater than or equal to the concentration in Table C.2-1

40 throughout each test to be representative of typical MWC 41

42 conditions. The fuel supply and air supply will also be adjusted as needed to approach the target H_2O concentration in exhaust gas in Table C.2-1.

3

The pyroprobe section final temperature (at end of 4 temperature ramp-up) will be 750 °C or as needed to assure 5 this section is 50 to 100 °C above the highest temperature for complete gasification across the test substance 7 composites as determined from the TGA results; see Section 8 C.2.3. This is necessary to assure complete gasification 9 of the sample of test substance composite and a common set 10 of experimental conditions across the test materials during 11 combustion testing. 12

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C.2.4.3.4 Blanks

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A minimum of one thermal blank will be run prior to each set of three combustion test runs for a given test substance composite. Each thermal blank run will be at the corresponding combustion test conditions with all feeds except for the test substance.

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C.2.4.4 Process Monitoring

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ATRS process parameters in Table C.2-2 will be monitored for each combustion test at key points during the test as noted in the table. Each combustion test will be a minimum of 5 minutes in duration. If the duration of a combustion test is greater than 15 minutes, each parameter in Table C.2-2 will be recorded at least once every 15 minutes.

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TABLE C.2-2. COMBUSTION TEST MONITORING

Key Time for Recording		
Before & after gasification		
Before & after gasification		
After gasification		
Before & after gasification		
Before & after gasification		
Before & after gasification		
Before & after combustion test		
Before & after combustion test		
Before & after gasification		

3.2 3.3

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Temperature-Inlet 1 will be recorded at the end of the temperature ramp-up for gasification to monitor the pyroprobe final temperature.

The flow rate of the exhaust gas routed to the bubblers (see Section C.2.4.5.2) will be determined based on the flow measurements listed in Table C.2-2.

4 5 6

The amount of material fed to the system will be verified by weighing the pyroprobe insert cartridge before and after each experiment.

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Exhaust gas monitoring is described in Section C.2.4.5.

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C.2.4.5 Exhaust Gas Monitoring

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Combustion exhaust gas will be continuously monitored for 13 oxygen during each combustion test via in-line MSD or via 14 an oxygen monitor. CO2 in exhaust gas will be monitored via 15 in-line GC, in-line MSD, or a continuous monitor; or 16 exhaust gas will be collected in Tedlar® bags for off-line 17 analysis of CO2. Carbon monoxide (CO) in exhaust gas will 18 be monitored via in-line GC or a continuous monitor; or 19 exhaust gas will be collected in Tedlar® bags for off-line 20 analysis of CO. Tedlar® bag samples may be collected at 21 the exit of the bubblers described in Section C.2.4.6. 22

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C.2.4.6 Exhaust Gas Sampling

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Gas samples for off-line analysis will be collected as described in Appendix D.1, revised as necessary pursuant to Appendix C.1.2.2 if applicable.

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A minimum of 60 mL of bubbler aqueous solution composite is expected from each combustion test. Of this, a minimum of 45 mL will be directed to PFOA analysis, and the remainder will be directed to fluoride ion analysis.

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C.2.4.7 Exhaust Gas Analysis

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C.2.4.7.1 Fluoride Ion

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A portion of the composite bubbler aqueous solution sample from each combustion test collected as described in Section C.2.4.6 will be analyzed for fluoride ion via ion chromatography using EPA Method 300.0.

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C.2.4.7.2 PFOA

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46 A portion of the composite bubbler aqueous solution sample 47 from each combustion test collected as described in Section

c.2-10

C.2.4.6 will be analyzed for PFOA via LC/MS/MS as described in Appendix D.2. 2 3 As described in Appendix D.2, composite bubbler aqueous 4 solution sample results less than method detection limit 5. (MDL) will be reported as not detected (ND), results 6 between MDL and the limit of quantitation (LOQ) will be 7 reported as not quantifiable (NQ), and numerical values 8. will not be reported. 9 10 Due to background levels of PFOA, the analytical laboratory 11 will only report numerical values for PFOA concentration in 12 the aqueous solution greater than or equal to the LOQ. 13 This is required to assure that the reported concentration 14 value is attributable to the aqueous solution sample rather 15 than to background. 16 17. C.2.5 Reporting of Results 18 19 C.2.5.1 Elemental Analysis Results 20 21 The results of elemental analysis for each test substance 22 composite (as noted in Section C.2.1) will be reported. 23 The laboratory reports will be included in an appendix to 24 the final report for incineration testing (test report). 25 26 C.2.5.2 Combustion Stoichiometry Results 27 28 Combustion stoichiometry (as noted in Section C.2.2) 29 calculations for each test substance composite will be 30 included in an appendix to the test report. 31 32 C.2.5.3 TGA Results 33 34 35 The temperature for complete gasification and the TGA graphical results for each test substance composite (as 36 37 noted in Section C.2.3) will be included in an appendix to 38 the test report. 39 Combustion Test Results 40 C.2.5.4 41 42 C.2.5.4.1 Process Monitoring 43 Process monitoring data (as noted in Section C.2.4.4) 44

C.2-11

recorded for each combustion test will be reported in

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tabular form.

1 C.2.5.4.2 Exhaust Gas Monitoring

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Exhaust gas O₂, CO and CO₂ monitoring results will be reported as the integrated or average value for each combustion test. CO will be reported in terms of parts per million by volume (ppmv). O₂ and CO₂ will be reported in terms of percent by volume (%).

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C.2.5.4.3 Exhaust Gas Analytical Results

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Results of analyses noted in Section C.2.4.7 will be reported for each replicate of each combustion test.

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The analytical result for each analyte in Section C.2.4.7
will be reported in terms of concentration (mass per
volume) in the bubbler aqueous solution. For each analyte,
this value will be used with the associated exhaust gas
volume to compute an exhaust gas concentration and with the
associated test substance mass to compute mass of analyte
per mass of test substance composite.

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C.2.5.4.3.1 Fluoride

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Fluoride ion in the exhaust gas will be reported on the basis of mass of fluoride ion per mass of test substance composite. The corresponding hydrogen fluoride value for each will also be computed and reported for reference.

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C.2.5.4.3.2 PFOA

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PFOA results for the bubbler aqueous solution samples will be reported as described in Section C.2.4.7.2. PFOA results for associated blanks will also be reported.

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36 37 If present in the bubbler aqueous solution at a concentration above the matrix-specific LOQ, PFOA in the exhaust gas will be reported on the basis of mass of PFOA per mass of test substance composite.

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C.2.5.5 Release Assessment

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In the event that PFOA is reported for the exhaust gas bubbler aqueous solution at a concentration at or above the LOQ (as defined in Appendix D.2) for two or more of the three runs for a given test substance composite, a release assessment report for the full-scale waste incineration of products represented by the test substance composite will

- 1 be prepared following the outline in Appendix E.2 and will 2 be included in the test report.
- 3
 4 C.2.5.6 Test Report Outline
- 5
 6 The outline for the test report is presented in Appendix
 7 E.3. All reporting discussed in Sections C.2.5.1 through
- 7 E.3. All reporting discussed in Sections C.2.5.3 8 C.2.5.5 will be included in this test report, as
- 9 applicable.

APPENDIX D.1 EXHAUST GAS SAMPLING VIA BUBBLERS

Gas samples for off-line analysis will be collected from a vent line off the interface of the thermal reactor system described in Appendix C.2.4. Flexible (silicone or equivalent) tubing will connect the vent line and a set of bubblers.

Gas absorption via these bubblers will provide aqueous solution (of documented content) to analyze for prescribed parameters. Two to four bubblers (low pressure drop impingers) in series will be used. Each bubbler will contain a predetermined amount of aqueous solution, and the total amount of solution at the beginning of each test run will be a minimum of 55 mL. The temperature of the gas exiting the last bubbler will be monitored.

An additional bubbler (which is empty) will be added to the front end of this series of bubblers to serve as a knock-out pot if calculations or preliminary measurements indicate that greater than 10 mL of water will be produced during the testing for a given material.

Upon completion of sample collection, the amount in each bubbler will be weighed and recorded, and the contents of the bubblers will be composited for subsequent analysis. Additionally, the flexible tubing will be rinsed with 5 mL of HPLC water to collect potential condensate in the tubing; this rinsate will be combined with the bubbler composite prior to analysis.

Bubbler aqueous solution composites will be conveyed to analytical laboratory(ies) in polyethylene, polypropylene, or glass container(s).

APPENDIX D.2 PFOA ANALYSIS BY LC/MS/MS

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D.2.1 Introduction

Appendix C.

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Samples to be analyzed for PFOA in this study will be subjected to Liquid Chromatography with Tandem Mass Spectrometry (LC/MS/MS) in accordance with "Method of Analysis for the Determination of Ammonium Perfluoroctanoate (APFO) in Water Revision 1" (Exygen method) revised per the section-by-section comments listed in Section D.2.4 below. These revisions are necessary to adapt a method originally developed for liter quantity water samples to samples related to testing described in

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The testing programs described in Appendix C are expected to generate samples of aqueous solution, methanol (e.g., as used for extraction or rinsing), and corresponding blanks. The expected sample size for aqueous solution samples (from exhaust gas bubbler sample collection) available for analysis via this method is approximately 50 mL.

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D.2.2 Method Summary

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PFOA is extracted from water using a disposable C₁₈ solid phase extraction (SPE) cartridge. PFOA is eluted from the cartridge with methanol. Quantification of PFOA is accomplished by electrospray liquid chromatography/tandem mass spectrometry (LC/MS/MS) analysis.

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D.2.3 Reporting

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The target limit of quantitation (LOQ) for this study with this method is 50 ng/L based on prior work with water samples where an 8-fold concentration via extraction using C₁₈ SPE cartridge has been demonstrated. The actual LOQ will be matrix dependent; for samples (e.g., methanol rinsate) where the 8-fold concentration cannot be performed, the target LOQ for this study is 400 ng/L.

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Sections 4.5.4 and 5 of the Exygen method explain reporting for field samples such as bubbler aqueous solution composites, which are distinct from blanks and spikes, as follows:

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Field samples in which either no peaks or peaks

less than the MDL are detected at the corresponding analyte retention time will be reported as ND (not detected). Samples in which peaks are detected at the corresponding analyte retention time that are less than the LOQ and greater than or equal to the MDL will be reported as NQ (not quantifiable).

Therefore, sample results less than method detection limit (MDL) will be reported as ND, and sample results between MDL and the limit of quantitation (LOQ) will be reported as NQ. Numerical values will not be reported for such samples. Only concentrations above the LOQ, where the reported concentration is attributable to the sample rather than to background, are reported with numerical values.

Additionally, if the PFOA anion is found in a sample at a concentration above the LOQ for the matrix but is less than 5 times the concentration found in the associated blank, the result will be reported, flagged, and treated as ND.

D.2.4 Study-Specific Comments on the Method

Section	Comment
1	• The concentration of PFOA found will be reported directly and the mathematical conversion for reporting as APFO mentioned in the 4 th sentence of the 2 nd paragraph will not be performed.
	• Since the 8-fold concentration described in the 2 nd sentence 4 th paragraph (which forms the basis for the LOQ in the 3 rd paragraph and the MDL in the 4 th paragraph) is dependent on having a minimum of 40 mL of aqueous sample amenable to extraction using the C ₁₈ SPE cartridge described in section 4.4 of the method, the LOQ and MDL in the method will be a factor of 8 higher than reported where less than 40 mL of sample is available or where the sample is not amenable to extraction using the
	C_{18} SPE cartridge described in section 4.4 of the method (e.g., methanol).
3.3 Note at top of page 8	 The note stating "Equivalent materials may be substituted for those specified in this method if they can be shown to produce satisfactory results" will not be used in the analysis for this testing program.

3.3	The following text will be used in place of
Notes,	Note 1 with respect to the PFOA analysis
Note 1	conducted for this testing program:
MOCE I	conducted for this testing program:
,	In order to avoid contamination, the use of
	disposable labware (tubes, pipets, etc.) is
	required.
3.3	The following text will be used in place of
Notes,	Note 4 with respect to the PFOA analysis
Note 4	conducted for this testing program:
	Solvents (e.g., methanol) used for this
	analysis must be checked for the presence
	of contaminants by LC/MS/MS before use.
3.5	Where the available amount of sample is
opening	expected to be much less than 1 liter,
text	I
	insufficient sample is available to prepare
prior to	the fortified matrix spikes described in the
3.5.1	opening text of section 3.5. In this case,
-	the analytical standards discussed in this
	opening text will be limited to two purposes
	since the third purpose (matrix spike) stated
	in the method cannot be done.
4.3,	 Where the available amount of sample is
item b	expected to be less than 80 mL (= 2 * 40), the
	replicate extraction noted in the first
	sentence of this item cannot be performed.
	 If the sample is not an aqueous sample
	amenable to extraction using the C_{18} SPE
	cartridge described in section 4.4 of the
	method, then section 4.4 is skipped such that
	_ ·
	the sample is analyzed directly. (Note: For
	such samples, the LOQ and MDL will be 8 times
	higher than the values quoted in the method.)
4.3,	As noted in comment on section 3.5 opening
item c	text above, fortified matrix spikes will not
	•
	be prepared when the available amount of
.	sample is much less than 1 liter.
,	Where the available amount of sample is
	expected to be less than 80 mL (= 2 * 40), the
	conditional repeat fortification and
	extraction described in the third sentence of
	this item cannot be performed.
4.4	• Extraction using the C ₁₈ SPE cartridge requires
	· · · · · · · · · · · · · · · · · · ·
	a suitable aqueous sample. This extraction
	and the corresponding 8-fold concentration

	pointed out in the NOTE at the end of this section cannot be performed on non-aqueous (e.g., methanol) samples.
4.4, item 1	• In order to measure out the 40 mL mentioned in this item, it is necessary to have at least 45 mL of sample to enable pipet transfer.
4.5.4, item g	• A storage stability study for PFOA in water performed independently of the development of the method indicates that PFOA may be stored in glass, polystyrene, polypropylene, or polyethylene containers without measurable degradation for up to 68 days prior to extraction. Therefore, the total holding time between sample collection and analysis for aqueous PFOA samples in this study may exceed the 14 day limit noted in the first sentence of this item provided that the sample is not held for greater than 68 days unless additional storage stability testing justifies a longer hold time.
4.6, item 3	• As noted in comment on section 3.5 opening text above, fortified matrix spikes will not be prepared when the available amount of sample is much less than 1 liter. In this case, acceptance criteria for matrix spike recoveries will not be considered.
5, item c	• The calculation in equation 3 in this section will not be performed since it is not necessary to convert the PFOA analytical results to APFO for this study.

D.2.5 Reference

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Flaherty, J. and K. Risha, "Method of Analysis for the Determination of Ammonium Perfluorooctanoate (APFO) in Water Revision 1", Exygen Method No. 01M-008-046 Revision 1, January 2003. (EPA Docket ID OPPT-2003-0012-0040)

APPENDIX D.3

WICKBOLD TORCH METHOD FOR TOTAL FLUORINE

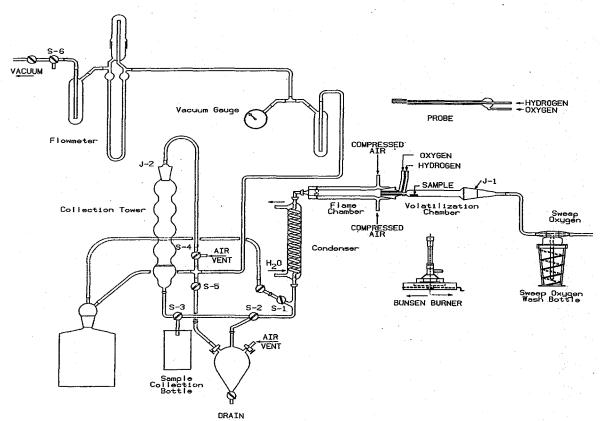
D.3.1 Introduction

 "The carbon-fluorine bond is exceptionally strong, and extremely vigorous conditions are needed for quantitative" analysis of fluorine in organic compounds. (Kissa, 1998) The "most vigorous" technique for measurement of fluorine in organic compounds is "combustion in an oxyhydrogen flame" referred to as the Wickbold torch. (Kissa, 1998)

D.3.2 Apparatus

A typical configuration for the Wickbold oxyhydrogen torch apparatus as described by Sweetser (1956) is shown in Figure D.3-1.

FIGURE D.3-1. WICKBOLD OXYHYDROGEN TORCH APPARATUS



D.3.3 Method Description The sample size for the standard sample boat is up to 20 mg 3 for a solid or up to 5 mL for a liquid. 4 5 With the oxyhydrogen torch in operation, the sample is б pyrolyzed or vaporized with a Bunsen burner moving on a 7 rail below the volatilization chamber. The vapors and 8 pyrolysis products are swept through the oxygen-hydrogen 9 flame chamber operating at up to approximately 2000 °C to 10 mineralize the fluorine in the sample to fluoride ion. 11 resulting fluoride ion is absorbed in the collection tower 12 containing water or an alkaline solution. 13 14 The absorbed fluoride ion is measured via fluoride ion-15 selective electrode or ion chromatography. 16 17 The reported limit of quantitation for total fluorine via 18 the Wickbold Torch method is 0.5 ppm (0.5 mg/kg). 19 accuracy of this method for determination of total fluorine 20 in fluorinated polymers is exemplified by total fluorine 21 values of 75.35% to 75.84% for PTFE with known total 22 fluorine content of 76.0%. (Sweetser, 1956) 23 24 D.3.4 Safety Considerations 25 26 Use of hydrogen presents a potential fire and explosion 27 28 hazard. Use of oxygen presents a potential fire hazard. Safe operation of the oxyhydrogen torch is assured by the 29 use of specialized equipment with shielding and elaborate 30 31 safety devices by well-trained personnel at a qualified 32 laboratory. 33 D.3.5 References 34 35 "Analysis of Anionic Fluorinated Surfactants", 36 Chapter 8 in Anionic Surfactants: Analytical Chemistry -37 2nd Edition, Revised and Expanded, edited by John Cross. 38 39 Marcel Dekker Surfactant Science Series, volume 73, 1998. 40

Sweetser, P. B. "Decomposition of Organic Fluorine

42 Compounds by Wickbold Oxyhydrogen Flame Combustion Method",

43 Analytical Chemistry, vol. 28, pp. 1766-1768, 1956.

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APENDIX D.4

WASTE INCINERATION AND OPERATION CONDITIONS

Polymers of the sort being investigated in this testing program may be present at trace to low concentrations in the feedstreams to municipal waste combustors and/or medical waste incinerators in the U.S.

D.4.1 Types of Incinerators

D.4.2.1 Municipal Waste Combustors

According to the Integrated Waste Services Association (IWSA), there are a total of 98 waste-to-energy facilities operating municipal waste combustors (MWCs) in the U.S. as of 2002. (IWSA 2002) Table D.4-1 summarizes the number and annual capacity of these units by type of technology employed.

Table D.4-1. MWCs in 2002

Type	Number of	Annual Capacity	Fraction
-1100	Facilities	(million Ton/year)	of Waste
Mass Burn	68	22.5	76.5%
Refused Derived	18	6.4	21.8%
Fuel (RDF)			
Modular	12	0.5	1.7%
Total	98	29.4	100.0%

D.4.1.2 Hospital/Medical/Infectious Waste Incinerators

Although earlier reports indicated approximately 2400 medical waste incinerators in the U.S. in the 1990s burning approximately 846 thousand tons of hospital and medical/infectious waste (EPA 1997), the current EPA Office of Air Quality, Planning, and Standards (OAQPS) inventory indicates that there are 116 hospital/medical/infectious waste incinerators (HMIWIs) in the U.S. as of July 28, 2003. (EPA 2003)

This represents a greater than 90% reduction in the number of operating HMIWIs in the U.S. Many medical waste incinerators were closed rather than upgraded to meet new emission standards, as hospitals improved their programs to segregate infectious ("red bag") waste burned in HMIWIs from non-infectious ("black bag") waste handled as municipal solid waste after it leaves the hospital.

40 Consequently, the amount of segregated infectious waste

burned in HMIWIs is expected to be less than 0.3 million
tons per year.

EPA notes that over 97% of medical waste incinerators are controlled air modular units (EPA 2000a). Recent communication with EPA OAQPS indicates that virtually all existing HMIWIs are controlled air modular (two-chamber) units.

D.4.2 Incinerator Operating Conditions

Many incinerators for municipal solid waste are designed to operate in the combustion zone at 1800 °F (982 °C) to 2000 °F (1093 °C) to ensure good combustion. (EPA 1995) EPA's new source performance standards (NSPS) and emission guidelines for both municipal waste combustors (MWCs) and hospital/medical/infectious waste incinerators (HMIWIs) are based on the use of "good combustion practices" (GCP). (EPA 1997, EPA 2000b, EPA 2000c, Van Remmen 1998)

Referring to MWCs, Donnelly notes, "Design of modern efficient combustors is such that there is adequate turbulence in the flue gas to ensure good mixing, a high-temperature zone (greater than 1000 °C) to complete burnout, and long enough residence time at high temperature (1-2 sec) for complete burnout." (Donnelly 2000) The term "flue gas" here refers to the gas above the grate.

With respect to HMIWIs, Van Remmen states "any unit which presently [prior to compliance date] has a [secondary chamber] residence time less than two seconds at 1000 °C does not meet the requirement for good combustion under the new regulations." (Van Remmen 1998)

 Similarly, most MWCs operate with a 2 second gas residence time in the high temperature zone in order to assure compliance with emission standards on carbon monoxide (CO) and dioxins.

40 D.4.2.1 MWC Operating Conditions

42 D.4.2.1.1 Mass Burn MWC

44 Review of the IWSA Directory (IWSA 2002) indicates that 45 almost all of these mass burn units are mass burn water 46 wall furnaces. Nearly all mass burn water wall furnaces 1 have reciprocating grates or roller grates to move the 2 waste through the combustion chamber. (EPA 1996a)

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Studies on the Millbury, Massachusetts mass burn water wall MWC produced gas temperature versus residence time results. (Scavuzzo, Strempek, and Strach 1990) Calculations based on Figure 6 of this paper indicate a time-averaged temperature of 2238 °F (1226 °C) over a 2 second. The corresponding gas temperature at the 2 second level from this figure is 1750 °F (954 °C).

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A report on the Warren County, New Jersey mass burn water 12 wall MWC indicates that the design gas temperature between 13 the grate and secondary air inject was greater than 2000 of 14 (1093 °C) over a gas residence time of an additional 2.2 15 seconds. (Schuetzenduebel and Nobles 1990) This report 16 17 also shows that this MWC was designed for 2 seconds residence time above 1800 °F (982 °C) between the 18 introduction of secondary air and the exit of the furnace 19 section. (Schuetzenduebel and Nobles 1990) The temperature 20 profile (Figure 21) in the temperature correlation test 21 report (Schutzenduebel 1989) for this MWC shows the full 22 load gas temperature at the secondary air injection point 23 is 2650 °F, and the gas temperature at the 2-second point is 24 1850 °F. Therefore, testing indicates an average 25 temperature of 2250 °F (1232 °C) over this 2 second gas 26 residence time for the Warren County unit. A related 27 report for the Warren County MWC by the design firm 28 indicates that the exhaust gas oxygen concentration is 29 nominally 10% (dry basis). (Blount Energy Resource Corp. 30 31 1989)

32 33

> 34 35

Information from these 2 MWCs demonstrates that the average gas temperature across a 2 second residence time for mass burn MWCs is conservatively expected to be greater than $1100\,^{\circ}\mathrm{C}$.

36 37

Test report data from a typical mass burn MWC (Fairfax, Virginia) indicates typical average furnace exit gas concentrations are 10.8% oxygen (dry basis) and 18.4% moisture (water). (Clean Air Engineering, 1997)

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As indicated in Table D.4.1, mass burn units account for over 76% of the municipal solid waste incinerated in the U.S.

1 2

D.4.2.1.2 RDF MWC

Furnace temperatures as well as flue gas oxygen and moisture (H_2O) levels for the Mid-Connecticut RDF combustor during performance tests while operating under good combustion conditions across a range of steam loads (Finklestein and Klicius 1994) are summarized in Table D.4-2.

Table D.4-2. RDF MWC - Mid-Connecticut

Steam load	low	low	inter- mediate	inter- mediate	normal	normal	normal	high
test number	PT-13	PT-14	PT-10	PT-02	PT-09	PT-08	PT-11	PT-12
Furnace temperature (°C)	965	1004	1012	1022	1033	1015	1026	1049
flue gas O ₂ (%)	10.1	9.6	9.2	9.1	7.6	7.5	7.9	6.4
flue gas moisture	12.4	11.1	12.3	15.4	15.1	16.3	14.1	16.2

The average operating conditions for this RDF unit across the range of steam loads are 1016 $^{\circ}\text{C}$, 8.4% O_2 (dry basis), and 14.1% moisture.

Examination of the report and MWC temperature monitoring practices indicates that these temperatures are effectively combustion zone exit temperatures. Therefore, in order to determine the average MWC combustion zone temperature across a 2 second gas residence time, it is necessary to understand the time-temperature profile of the MWC.

 Since waste combustion in this and most other RDF units in the U.S. involves burning on the grate (EPA 1996a) similar to the operation of mass burn MWCs, the time-temperature profile in an RDF unit is expected to be similar to that described in Section D.4.2.1.1 above. Based on this similarity and the temperatures in Table D.4-2, the average gas temperature across a 2 second residence time for RDF units is conservatively expected to be greater than 1100 °C.

As indicated in Table D.4.1, RDF units account for approximately 22% of the municipal solid waste incinerated in the U.S.

D.4.2.1.1 Modular MWC

Modular MWCs are generally small dual-chamber units, accounting for less than a total of 2% of the municipal solid waste incinerated in the U.S. in 2002. Modular MWCs are generally equipped with auxiliary fuel burners in the

secondary chamber. (EPA 1996a) EPA notes that the secondary chamber exit temperature of modular MWCs is maintained at typically 980 to 1200 °C. (EPA 1996a)

5 A typical modular MWC in Polk County, Minnesota is operated 6 with a gas residence time of 2 seconds, in the secondary 7 chamber, a secondary chamber exit temperature in the range 8 of 1800 °F (982 °C) to 2000 °F (1093 °C), flue gas oxygen 9 concentrations in the range of 10% to 13% (dry basis), and 10 flue gas moisture in the range of 10% to 15% (Pace 11 Analytical 2003).

Since the secondary chamber exit temperature is expected to be the minimum gas-phase temperature for the chamber, the secondary chamber average gas temperatures for modular MWCs are expected to be 1000 °C or greater.

As indicated in section D.4.1, such modular units are generally small MWCs and account for less than a total of 2% of the municipal solid waste incinerated in the U.S.

D.4.2.1.4 MWC Summary

Considering the relative quantities of municipal waste burned annually in each type of MWC and the data in this section, typical operating conditions for the high temperature zone of most MWCs are >1000 $^{\circ}$ C average temperature across 2 second residence time with exit gas concentrations of 10% O_2 (dry basis) and >15% moisture.

D.4.2.2 HMIWI Operating Conditions

The range of temperatures for the secondary chamber of controlled air medical waste incinerators has been reported as 980 to 1200 °C. (Theodore 1990) EPA notes that auxiliary fuel (e.g., natural gas) is burned in the secondary chamber of medical waste incinerators to sustain temperatures in the range of 985 to 1095 °C and that combustion air at 150 to 250 % of the stoichiometric requirement is usually added to the secondary chamber. (EPA 2000a, EPA 1994a)

In its model plant description background document, EPA
notes that the average moisture content in HMIWI flue gas
was about 10 % based on available data, and EPA states
"limited data show that older [HMIWI] units typically have
residence times that range from essentially 0 seconds up to
about 1 second." (EPA 1994b) However, as noted above, a

D.4-5

- more recent report indicates that HMIWIs still in operation have secondary chamber temperatures greater than or equal 2 to 1000 °C with a gas residence time of 2 seconds. (Van 3 Remmen 1998) For example, EPA studied the incinerator at 4 5 Weeks Hospital in New Hampshire as a typical HMIWI with a design residence time of 2 seconds in the secondary 6 7 chamber. (EPA 1996b) During this testing, the average exit secondary chamber exit temperature was 1024 °C, and the flue 8 gas oxygen concentration was 13.5%. (dry basis) (EPA 1996b) 9
- Review of test reports for all HMIWIs in the EPA docket for 11 the HMIWI NSPS and EG rulemakings that are listed in EPA's 12 current HMIWI inventory (EPA 2003) does not refute Van 13 Remmen's statement above on residence time and temperature 14 and indicates HMIWI flue gas oxygen concentrations for 15 these units in the range of 10 to 15% (dry basis) and stack 16 17 moisture concentrations as high as 30% (after wet (Environmental Laboratories Inc. 1993, EPA 18 scrubbing). 1996, HDR Engineering 1994a, HDR Engineering 1994b, METCO 19 Environmental 1992, Technical Services, Inc. 1993, 20 Technical Services, Inc. 1994a, Technical Services, Inc. 21 Apparently, the older HMIWIs referred to in EPA's 22 model plant description background document either have 23 been shut down or upgraded to operate with secondary 24 chamber exit temperatures higher than 1000 °C at a gas 25

Secondary chamber temperature of HMIWIs is monitored near the secondary chamber outlet. (EPA 1994) Hence, when the auxiliary burner (located on the end opposite from the outlet) is in use, the average gas temperature in an HMIWI secondary chamber is greater than the outlet temperatures noted above. Therefore, secondary chamber average gas temperatures for HMIWIs are expected to be 1000 °C or greater with a gas residence time of 2 seconds.

In summary, typical operating conditions for the secondary chamber of operating HMIWIs in the U.S. are 1000 $^{\circ}$ C average temperature across 2 second residence time with exit gas concentrations of 13% O_2 (dry basis) and >10% moisture.

D.4.3 Pollution Control Equipment

residence time of 2 seconds.

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Over 99% of large MWC capacity operates with a spray dryer absorber/scrubber. (IWSA 2003) Approximately 80% of large MWC capacity operates using carbon injection as part of the pollution control system. (IWSA 2003) Due to requirements

in the NSPS (EPA 2000b) and EG (EPA 200c) for small MWCs, 1 small MWCs planning continued operation are generally 2 upgrading or have upgraded their pollution control 3 equipment to add spray dryer absorbers or other acid gas 4 control and carbon injection. 5

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Review of EPA's HMIWI inventory (EPA 2003) indicates that essentially all HMIWIs have some form of wet or dry scrubbing for acid gas control.

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D.4.4 Summary

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Approximately 30 million tons per year of municipal solid waste was combusted in the United States annually in wasteto-energy municipal waste combustors in 2003. Approximately 0.3 million tons per year of segregated

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medical waste was combusted annually in the United States 17

in hospital/medical/infectious waste incinerators in 2003. 18

Considering the relative amounts of waste combusted 19 annually, typical operating conditions for waste 20

incineration in the U.S. across these two classes of units 21

22 are as follows:

23

Average Temperature	>1000 °C
Residence Time	>2 sec
O2 concentration in exhaust gas	$\overline{1}$ 0% (dry basis)
H ₂ O concentration in exhaust gas	15%

24

EPA emission regulations currently in place or in place by 25 2005 require that operating municipal waste combustors and 26 hospital/medical/infectious waste incinerators have or will 27 have air pollution control equipment such as wet or dry 28 scrubbing for acid gas control. 29

30

References 1 2 Blount Energy Resource Corp. Correlation Procedure for 3 Continuously Monitoring Furnace Temperatures (Warren County Resource Recovery Facility), March 22, 1989. 5 6 Clean Air Engineering. Test Report for Covanta of Fairfax, 7 Inc. I-95 Energy/Resource Recovery Facility, 1997. 8 9 Donnelly, J.R. Waste Incineration Sources: Municipal Waste 10 Combustion. In: W.T., ed., Air Pollution Engineering 11 Manual, 2nd edition. Air and Waste Management Association. 12 New York, NY: Van Nostrand Reinhold, 2000, pp 257-268. 13 14 Environmental Laboratories Inc. Stack Test Report for 15 Emissions Testing of the Bethesda Memorial Hospital Waste 16 17 Incinerator, Boynton Beach Florida, September 13, 1993. 18 Environmental Protection Agency (EPA). Municipal Waste 19 Combustion Assessment: Technical Basis for Good Combustion 20 Practice, EPA 600/8-89-063, August 1989. 21 22 Medical Waste Incinerators - Background Information 23 EPA. for Proposed Standards and Guidelines: Control Technology 24 Performance Report for New and Existing Facilities, EPA-25 453/R-94-044a, July 1994. 26 27 Medical Waste Incinerators - Background Information 28 -EPA. for Proposed Standards and Guidelines: Model Plant 29 Description and Cost Report for New and Existing 30 31 Facilities, EPA-453/R-94-045a, July 1994. 32 EPA. Decision Maker's Guide to Solid Waste Management, 33 Volume II, Chapter 8, 1995. 34 35 AP-42, Fifth Edition, Volume I, Chapter 2: Solid 36 Waste Disposal, Section 2.1, Refuse Combustion, Supplement 37 B, October 1996. 38 39 40 Medical Waste Incineration Emission Test Report:

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44 EPA. Standards of Performance for New Stationary Sources

Weeks Memorial Hospital, Lancaster, New Hampshire, EMC

45 and Emission Guidelines for Existing Sources:

46 Hospital/Medical/Infectious Waste Incinerators, 62 Federal

47 Register 48346, September 15, 1997.

Report 96-MWI-11, March 1996.

Exposure and Human Health Reassessment of 2,3,7,8-2 EPA. Tetrachlorodibenzo-p-Dioxin (TCDD) and Related Compounds, 3 Part I: Estimating Exposure to Dioxin-Like Compounds Volume 4 2: Sources of Dioxin-Like Compounds in the United States, Chapter 3, EPA/600/P-00/001Bb, Draft Final Report, 6 September 2000. 7 8 New Source Performance Standards for New Small 9 Municipal Waste Combustion Units, 65 Federal Register 10 76350, December 6, 2000. 11 12 Emission Guidelines for Existing Small Municipal 13 Waste Combustion Units, 65 Federal Register 76378, December 14 15 6, 2000. 16 17 EPA. HMIWI Facility and Emissions Inventory, draft, July 18 28, 2003, www.epa.gov/ttnatw01/129/hmiwi/2003hmiwi_inventory.xls 19 20 Finklestein, A. and R. D. Klicius. National Incinerator 21 Testing and Evaluation Program: The Environmental 22 Characterization of Refuse-derived Fuel (RDF) Combustion 23 Technology, Mid-Connecticut Facility, Hartford, 24 Connecticut, EPA-600/R-94-140 (NTIS PB96-153432), December 25 26 1994. 27 28 HDR Engineering. Performance Test Results Report Submittal: Incinerator Waste Management Facility, Mayo 29 Foundation, Rochester, Minnesota, June 7, 1994. 30 31 HDR Engineering. Performance Test Results Report 32 Supplemental Submittal Charts, Data Sheets, Operator Log, 33 CEMS Data: Incinerator Waste Management Facility, Mayo 34 Foundation, Rochester, Minnesota, June 10, 1994. 35 36 37 Integrated Waste Services Association (IWSA). The 2002 IWSA Directory of Waste-to-Energy Plants, 2002, 38 39 www.wte.org/2002_directory/IWSA_2002_Directory.html 40 41 Air Pollution Control Devices on Operating Waste-to-42 Energy Plants: Year 2002, 2003. 43 44 METCO Environmental. Source Emissions Survey of University 45 of Texas Medical Branch, Incinerator Number 2 Exhaust Duct, Galveston, Texas, TACB Permit C-18655 for Clever Brooks, 46 July 1992. 47

1 Midwest Research Institute. Updated Hospital/Medical/ 2 Infectious Waste Incinerator Inventories Received from 3 Various Regions, States, and Counties, January 27, 1999. 4 5 Pace Analytical. Comprehensive Emissions Test Report: MSW 6 Incinerator Unit No. 1 ESP Outlet & MSW Incinerator Unit 7 No. 2 ESP Outlet (Polk County Solid Waste Plant), March 11-8 9 14, 2003. 10 11 Scavuzzo, S. A., J. R. Strempek, and L. Strach. 12 Determination of the Thermal Operating Characteristics in the Furnace of a Refuse-Fired Power Boiler" in Proceedings 13 of the 1990 National Waste Processing Conference, American 14 15 Society of Mechanical Engineers (ASME), 1990, pp. 397-404. 16 17 Schuetzenduebel, W. G. and W. C. Nobles. "New Jersey's 18 First Resource Recovery Facility (The Warren County Energy Recovery Facility)" in Proceedings of the 1990 National 19 20 Waste Processing Conference, ASME, 1990, pp. 321-343. 21 Schuetzenduebel, W. G. Blount Energy Corporation Report -22 Furnace/Boiler Temperature Correlation: Warren County 23 Resource Recovery Facility, Oxford, New Jersey, October 24 25 1989. 26 Technical Services, Inc. Source Test Report: Boca Raton 27 Hospital, Boca Raton, Florida, March 31-April 2, 1993. 28 29 30 Technical Services, Inc. Source Test Report: Mercy 31 Hospital South Miami, Florida, July 27-28, 1994. 32 Technical Services, Inc. Source Test Report: St. Vincent's 33 34 Medical Center Jacksonville, Florida, August 30, 1994. 35 Theodore, L. Air Pollution Control and Waste Incineration 36 for Hospitals and Other Medical Facilities, Van Nostrand 37 38 Reinhold, New York, 1990, pp 313-320. 39 Van Remmen, T. Evaluation of the available air pollution 40 control technologies for achievement of the MACT 41 42 requirements in the newly implemented new source performance standards (NSPS) and emission guidelines (EG) 43

for hospital and medical/infectious waste incinerators,

Waste Management, 1998, Vol. 18, pp 393-402.

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1	APPE	ENDIX E.1 (Fluoropolymers)
2	OUTI	INE FOR INTERIM PROGRESS REPORTING
3		
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5	Titl	taran da antara da a
6		Scale Incineration Testing of Fluoropolymers -
7		Interim Report
8		1 / TD M
9	OPPL	Docket ID No: OPPT-2003-0071
10		C. T. I. I. Davidski F. Jahra J.
11	Date	e of Interim Report: [date]
12		
13		
14		
15	This	Report covers the period from [date] to [date]
16		
17	4.	The state of almost the second parts and the second parts are second parts.
18	1)	List or description of significant ECA Test Program
19		milestones during this period:
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21		
22		
23		
24	0.)	prominting of Difficulties (TF new indicate area)
25	2)	Description of Difficulties: (If none indicate N/A)
26		
27		
28		
29		
30 .		
31		
32	2.	Tables below in manages to difficulting to
33	3)	Actions taken in response to difficulties: If none
34		indicate N/A)
35		
36		
37		
88		
39		
10	4.5	
11	4)	Other information relevant to the progress of the
12		testing program: (If none indicate N/A)

APPENDIX E.2 OUTLINE FOR RELEASE ASSESSMENT REPORT

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As described in Appendix C.2.5.5 of this ECA, if PFOA is reported for the exhaust gas bubbler aqueous solution at a concentration at or above the LOQ (as defined in Appendix D.2) for two or more of the three runs for a given test substance composite, then the potential for release from full-scale municipal and/or medical waste incineration, as applicable, (including application of air pollution controls) of products represented by the test substance composite in the United States will be assessed to put the data into perspective. At a minimum, the report will follow the general outline described below and will state assumptions, document the basis for the assumptions made, quantitatively estimate the variability of calculated estimates (based on the variability of the parameters in the evaluation), and qualitatively discuss the uncertainty of calculated estimates.

19 20 21

1.0 Introduction

22 23

• Statement of objective for combustion testing of test substance composites.

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 Applicability of the laboratory-scale combustion testing to full-scale municipal waste combustors (MWCs) and/or medical waste incinerators (as applicable) in the United States.

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2.0 Summary of study results

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• A listing of exhaust gas analytical results reported for each applicable test substance composite.

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 A listing of test substance composite analytical results reported for each applicable test substance composite.

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3.0 Discussion

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• Description of the combustion section of the applicable waste incineration process(es) being evaluated (MWC and/or medical waste incinerator) including the rationale for selecting test target temperature(s) and description of typical

E.2-1

operational parameters. Cross-reference to or submission of relevant parts of Appendix D.4 of this 2 ECA can satisfy this provision. 3 4 • Description of the post-combustion air pollution 5 control equipment (e.g., lime scrubbing, carbon 6 adsorption) employed by typical operating full-scale 7 waste incineration process(es) as applicable. 8 9 4.0 Extrapolation of laboratory test results to the 10 typical waste incineration process(es), as applicable, 11 described in Section 3.0 (above) for each test 12 substance composite to be evaluated. 13 14 The relevance of the subject test substance 15 composite to MWCs and/or medical waste incinerators. 16 17 The estimated concentration of the subject test 18 substance composite to the applicable type(s) of 19 waste incinerator. Available information on 20 hydrogen fluoride concentration in waste incinerator 21 exhaust can provide the basis for an upper bound on 22 this estimated concentration. 23 24 A description of the extrapolation. 25 26 • A description of any assumptions used. 27 28 • Any unique qualitative or quantitative descriptors 29 of the test, the testing equipment, and the results 30 deemed necessary for informative review of the test 31 and test results. 32 33 34 5.0 Sensitivity Analysis 35 36 Assessment of the impact of variability (quantitative) and uncertainty (qualitative) in each 37 38 parameter on the evaluation results.

6.0 Conclusions

7.0 References

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1	APPENDIX E.3	회사가 지점	
2	OUTLINE OF TEST REPORT*,**		
3			
4			
5	Table of Contents		
6			
7	Executive Summary		
8			
9	Introduction		
10			
11	I. Phase I PFOA Transport Testing		
12			
13	1. Experimental Apparatus		
14	2. Description of Test Conditions (including	ng deviations	
15	from protocol)		
16	3. Documentation of PFOA Standard		
17	4. Analytical Results	•	
18	4.1 PFOA		
19	4.2 Total Fluorine		
20	5. Transport Efficiency		
21	5.1 PFOA		
22	5.2 Total Fluorine		
23	6. Discussion of Results		
24	7. Conclusions		
25			
26	II. Phase II Incineration Testing (provided Phase	se II is performe	d)
27			
28	1. Documentation of Test Substance Composit	es	·
29	2. Elemental Analysis Results		
30	3. Combustion Stoichiometry Results		
31	4. TGA Results		
32	5. Combustion Testing		
33	5.1 Experimental Apparatus		
34	5.2 Description of Test Conditions (inc	luding deviations	ļ .
35	from protocol)		
36	5.3 Combustion Testing Results		
37	5.3.1 Process Monitoring		
38	5.3.2 Exhaust Gas Monitoring		j j
39	5.3.2 Exhaust Gas Sampling and Analy	vsis	u kg
40	5.3.2.1 PFOA		j.
41	5.3.2.2 Fluoride		
42	5.4 Discussion of Results		
43	5.5 Conclusions		
44			
45	III. Appendices		
46	tit. The citation .		
	Onelita Assumance Denset (-)		
47	Quality Assurance Report(s)		

1		
2		• Report(s) from Compositing Facility(ies) (provided Phase II
3		is performed)
4		
5		Reports from Analytical Laboratories
6		
7		 Release Assessment per Appendix E.2, if applicable
8		
9		
10		
11.	*	Test Report will include this information (as applicable)
12		but not necessarily in this order.
13		
14	**	References to literature in this report will include full
15		citations.

APPENDIX F

UNITED STATES ENVIRONMENTAL PROTECTION AGENCY

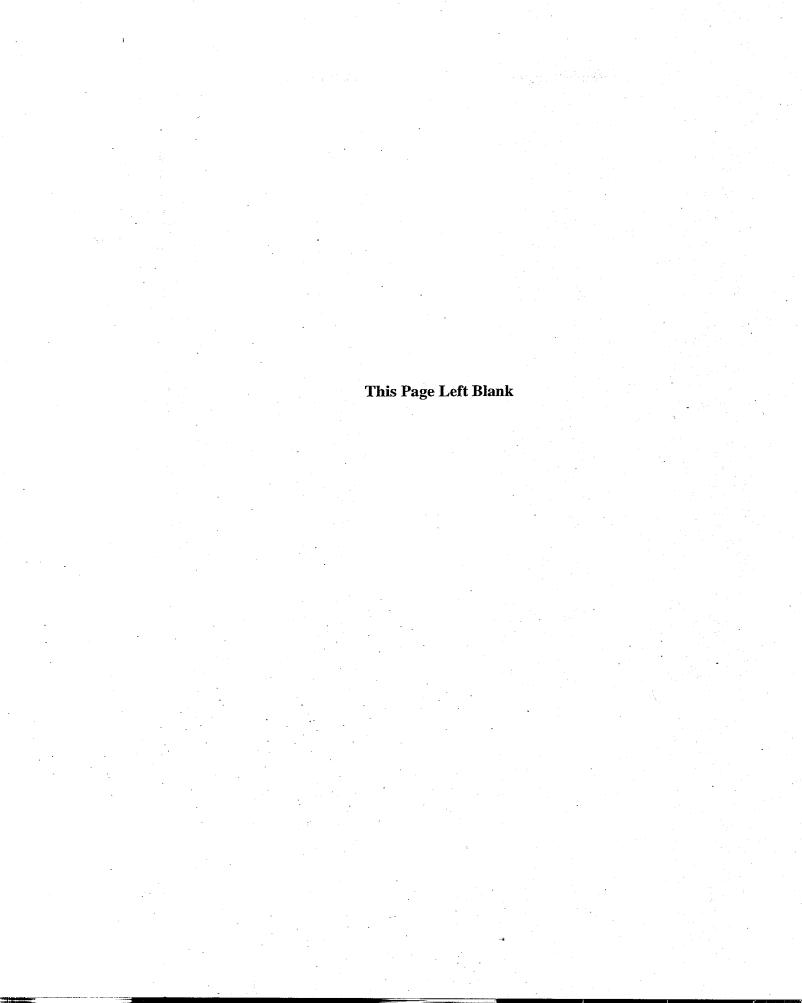
TESTING CONSENT ORDER FOR THE LABORATORY-SCALE INCINERATION TESTING OF FLUOROPOLYMERS

EPA Docket No. OPPT - 2003 - 0071

Under the authority of section 4 of the Toxic Substances Control Act (TSCA), 15 U.S.C. 2603, the United States Environmental Protection Agency (EPA) issues this testing consent order (Order) to take effect on the date of publication of the notice in the <u>Federal Register</u> announcing the issuance of this Order. This Order incorporates the enforceable consent agreement (ECA) for the laboratory-scale incineration testing of the fluoropolymer test substance composites listed in Appendix A of the ECA.

Date

Susan B. Hazen
Principal Deputy Assistant Administrator
Office of Prevention, Pesticides and Toxic Substances



TAB#3

Company Specific Signature Pages Containing Confidential Business Information

The Company specific signature pages contained in this section of the ECA are not publically available because one or more of the Signatory Companies have asserted that information contained on these pages is considered by them to be entitled for protection as TSCA confidential business information (CBI) (see Part XIV. D. of the ECA regarding confidentiality of information). The sanitized version of the signature pages are available in the Public Version of this document under TAB #3 (see Part XXIV of the ECA).

TAB#4

Replacement Pages for AGC Chemicals Americas, Inc.²

²Additional changes and corrections to the ECA document were identified after completion of the Public Review Process. EPA set in place a process whereby the needed changes(s) were made using strike-out with hand written correction(s) on each page (i.e., replacement page) of the ECA where such changes were needed. Each signatory was asked to acknowledge their concurrence by initialing and dating every change on each ECA replacement page. The ECA document contained under TAB # 1 contains the replacement pages originated by EPA. The pages under this Tab contain those replacement pages co-initialed by EPA and AGC Chemicals Americas, Inc.

Contains No Confidential Business Information

100 me w 140

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1/25/55 W 1410 Aqueous Fluoropolymer Dispersions Composite #4: (containing: - Ethene, tetrafluoro-, polymer-with trifluoro(pentafluoroethoxy) ethene, CAS No. 31784-04-0; Ethene, tetrafluoro-, homopolymer, CAS No. 9002-84-0; 1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene), CAS No. 25067-11-2; Propane, 1,1,1,2,2,3,3-heptafluoro-3- [(trifluoroethenyl)oxy]-, polymer with tetrafluoroethene, CAS No. 26655-00-5; Ethene, tetrafluoro -polymer with trifluoro(pentafluoroethoxy)cthene, CAS No. 31784-04-0; 1-Propene, 1,1,2,3,3,3- hexafluoro-, polymer with 1.1-difluoroethene and tetrafluoroethene, CAS No. 25190-89-0; and polytetrafluoroethylene, DCN No. 6304000001807.8

The procedure for constructing each composite is described in Appendix A.4. The polymer components for each composite will be unfilled first quality product polymer. substantially free of inorganic constituents. Each component of the four composites to be tested under this ECA will be accompanied by a certificate of analysis showing it to meet applicable product specifications.

OBLIGATION OF SIGNATORY COMPANIES ш.

- A. The Companies are bound by the terms of this ECA as specified below.
- Each Company shall be responsible for supplying the test substance(s) it manufactures for incorporation into the composite(s) to be tested under this ECA, as specified on each Company signature page and in Appendix A.3. The schedule for the testing program includes the deadline date by which the Companies must submit their contribution(s) to the facility(ies) that will be assembling the composites to be tested under this ECA. Any Company failing to comply with this ECA requirement will be in violation of this ECA as described in 40 CFR 790.65 (see Part XII of this ECA). In the event that one or more of the Companies are in violation as described above then the remaining Companies will inform EPA of the problem and request an EPA determination on how to proceed with the testing program described under this ECA. Each Company required to contribute to a particular composite is obligated to complete the testing required by this ECA for that composite. A Company shall not be responsible for any failure to perform its obligation under this ECA that is caused by circumstances beyond its control, that the Company could not have prevented through the exercise of due diligence.

⁸ EPA uses a variety of numerical identification systems for tracking chemicals. These include Chemical Abstract Service Registry numbers (CAS) (assigned to non-confidential listed chemicals), pre-manufacture notice (PMN) numbers (assigned by EPA when chemicals enter EPA's new chemical review process, document control numbers (DCN) (assigned by the Confidential Business Information Center for EPA tracking), and Accession (ACC) numbers (provided by EPA when a chemical identity requires protection as TSCA CBI). In addition, Polymer Exemption products will not have a TSCA Inventory ID number but may have a commercial trade identity.

to seek judicial review of any rule that may be adopted by EPA that imposes requirements to test any of the fluoropolymer chemicals listed in Appendix A.1 to this ECA.

XXII. RESERVATION OF RIGHTS BY COMPANIES

By signing this ECA, the Companies are not admitting that the requirements of TSCA Section 4 have been satisfied for promulgating a test rule to generate the data required by this ECA.

The Companies contend that the documents generated for the incineration testing program under this ECA are protected from public disclosure under 5 U.S.C. section 552(b)(4) and 15 U.S.C. section 2613(a) and do not constitute studies subject to disclosure under 15 U.S.C. section 2613(b). Accordingly, the public information disclosure provisions of this ECA are, in the view of the Companies, a waiver of legal rights.

XXIII. IDENTITY OF THE COMPANIES AND PRINCIPAL TEST SPONSOR

The Principal Test Sponsor is:

Fluoropolymer Manufacturers Group Allen Weidman The Society of the Plastics Industry, Inc. 1801 K Streert, N.W., Suite 600K Washington, DC 20006 202-974-5233

The Companies subject to this ECA are:

AGC Chemicals Americas, Inc. 229 East 22nd Street, Bayonne, NJ 07002

Daikin America, Inc. 20 Olympic Drive, Orangeburg, NY 10962 Dyneon, LLC 6744 33rd Street, Oakdale, MN 55128

E.I. du Pont de Nemours and Company

-Route 141 and Henry Clay / 1007 MARKET STRE

Wilmington, DE 19880-0711 / 1989

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Contains No Confidential Business Information

XXIV. SIGNATURE

TEST SPONSOR Dyneon, LLC 1, 2

Company technical contact person for handling correspondence marked as "Confidential"

Name:

George H. Millet

Title:

Director, Quality, Environment, Health and Safety

Address:

6744 33rd Street, Oakdale, MN 55128

Phone Number:

651-733-5637

	ECA S	ubject Chemicals fo	or Dyneon, LLC *
Entry	Composite	CAS Registry #	CAS 9CI Name
1	Dry non-melt Fluoropolymer Resin	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer
2	Dry non-melt Fluoropolymer Resin	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- (trifluoroethenyl)oxy]-, polymer with tetrafluoroethene
3	Dry melt Fluoropolymer Resin	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene
4	Dry melt Fluoropolymer Resin	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- [(trifluoroethenyl)oxy]-, polymer with tetrafluoroethene
5	Dry melt Fluoropolymer Resin	CAS #25190-89-0	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with 1,1-difluoroethene and tetrafluoroethene
6	Dry melt Fluoropolymer Resin		

10/8/04

10/8/64

Data in the table lists the chemical(s) and composite contributions for which Dyneon, LLC is responsible. The Company developed these data in response to EPA's letter of January 6, 2004. There is both a Public and CBI version of this page because the Company has asserted that data in this table are considered by them to be entitled to treatment as TSCA confidential business information (CBI) (see Part XIV. D. of this ECA regarding confidentiality of information).

² Dyneon, LLC is obligated under this ECA to perform Phase I PFOA Transport Testing (see Part III. C. and VII.A. of this ECA).

XXIV. SIGNATURE

TEST SPONSOR

E.I. du Pont de Nemours and Company 1, 2

Company technical contact person for handling correspondence marked as "Confidential"

Name:

David W. Boothe

Title:

Strategic Planning Manager - DuPont Fluorosolutions

Address:

Route 141 & Henry Clay, Wilmington, DE 19880-0711 19805 302-999-4091

4417 Lancaster Pike

Phone Number:

Chestrat Run 702

ECA Subject Chemicals for E. I. du Pont de Nemours and Company Entry Composite CAS Registry # **CAS 9CI Name** CAS #9002-84-0 Dry non-melt Ethene, tetrafluoro-, homopolymer 1 Fluoropolymer Resin Dry melt CAS #25067-11-2 1-Propene, 1,1,2,3,3,3-hexafluoro-, 2 polymer with tetrafluoroethene Fluoropolymer Resin CAS #26655-00-5 3 Dry melt Propane, 1,1,1,2,2,3,3-heptafluoro-3-(trifluoroethenyl)oxy]-, polymer with Fluoropolymer Resin tetrafluoroethene CAS #31784-04-0 Ethene, tetrafluoro-, polymer with 4 Dry melt Fluoropolymer Resin trifluoro(pentafluoroethoxy)ethene **Aqueous Dispersion** CAS #9002-84-0 Ethene, tetrafluoro-, homopolymer 5. 6 Aqueous Dispersion CAS #25067-11-2 1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene CAS #26655-00-5 7 Aqueous Dispersion Propane, 1,1,1,2,2,3,3-heptafluoro-3-(trifluoroethenyl)oxyl-, polymer with tetrafluoroethene

¹ Data in the table lists the chemical(s) and composite contributions for which E.I. du Pont de Nemours and Company is responsible. The Company developed these data in response to EPA's letter of January 6, 2004.

² E.I. du Pont de Nemours and Company is not obligated under this ECA to perform Phase I PFOA Transport Testing (see Part III. C. and VII.A. of this ECA).

Continued: ECA Subject	Chemicals for Dyneon, LLC
------------------------	---------------------------

Entry	Composite	CAS Registry #	CAS 9CI Name
7	Dry melt Fluoropolymer Resin	CAS #35560-16-8	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with ethene and tetrafluoroethen
8	Dry non-melt Fluoroelastomer Gum	CAS #27029-05-6	1-Propene, polymer with tetrafluoroethen
9	Dry non-melt Fluoroelastomer Gum	CAS #54675-89-7	1-Propene, polymer with 1,1- difluoroethene and tetrafluoroethene
10	Dry non-melt Fluoroelastomer Gum	CAS #26425-79-6	Ethene, tetrafluoro-, polymer with trifluoro(trifluoromethoxy) ethene
11	Dry non-melt Fluoroelastomer Gum	CAS #9010-75-7	Ethene, chlorotrifluoro-, polymer with j, difluoroethene
12	Dry non-melt Fluoroelastomer Gum	><	
13	Aqueous Dispersion	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer
14	Aqueous Dispersion	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene
15	Aqueous Dispersion	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- [(trifluoroethenyl)oxy]-, polymer with tetrafluoroethene
16	Aqueous Dispersion	CAS #25190-89-0	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with 1,1-difluoroethene and tetrafluoroethene

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APPENDIX A.3 COMPOSITION OF COMPOSITES TO BE TESTED

The four composite test substances for this test program are presented below in Table A.3-1 with the fluoropolymer types, CAS numbers, and associated monomers for these fluoropolymers. Each fluoropolymer used in each relevant test substance composite will have been made using APFO.

Table A.3-1. Test Substance Composites by Type

Test Substance	Fluoropolymer Type	CAS Mumber	Associated Monomers
Composite 1 -	PTFS	9002-84-0	LER
Dry non-melt resin	Modified PTFE	26653-00-5	TFE, PPVE
Composite 2 -	FBP	25067-11-2	IFE, HEP
Dry melt resins	PTA	26655-00-5 31784-04-0	TFE, PPVE TFE, PEVE
•	THV	25190-89-0	IFE, HEP, VDF
•	ETFE	68258-85-5	FFE, E
ng girth ng ng	HUB	35560-16-8	TFE, HFP, E
Composite 3 - Fluoroelastomers	Fluoroelastomer Copolymers	9011-17-0	VDP, HFP
	Fluoroelastomer Terpolymers	25190-89-0	TFE, HFP, VDF
	Base resistant elastomers	54675-89-7, 27029-05-6	TFE, VDF, P TFE, P
	Perfluoroelastomers	26425-79-6	TFE. PMVE
	CTFE elastomers	9010-75-7	CIFE, VED
	Low temperature elastomers	CBI	ife, Voe
Composite 4 - Aqueous	PTFZ	9002-84-0	TFE
Dispersions	FBP	25067-11-2	IFE, HFP
. 🕶	PFA	26655-00-5 31704-04-0	TFE, PPVE
	<u> Env</u>		TPE, PEVE TPE, HFP, VDF

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Confidential business information (CBI) regarding the chemical identity of low temperature elastomers has been submitted to EPA under separate cover.

Contains No Confidential Business Information

4.2.2 Composite 2

FEP, PFA ETFÉ

EEP, PEA, THV, ETEE, and HTE dry melt resins are available in powder form. Equal weights Vislay of the powder form of each component (following the approach in the example for Composite Z in Section 4.1 above) will be mixed together in dry form to yield Composite 2.

4.2.3 Composite 3

Fluoroelastomers are available in slab, lump, or sheet form. Composite 3 will be prepared following one of the following approaches:

a) Equal weights of each component (following the approach in example for Composite Z in Section 4.1) will be mixed on a rubber mill to produce a homogenous slab of preset thickness to yield Composite 3.

Or

b) Each component of Composite 3 will be cyrogenically cooled (to make the elastomers brittle) and size-reduced (e.g., ground) to produce powder. Equal weights of the powder form of each component (following the approach in the example for Composite Z in Section 4.1) will be mixed together in dry form to yield Composite 3.

4.2.4 Composite 4

Aqueous dispersions of PTFE, FEP, PFA, and THV are available as dispersions containing 20 to 60% fluoropolymer solids by weight. Composite 4 will be prepared following one of the following approaches:

a) Equal weights (on a dry solids basis) of each component in aqueous dispersion form (following the approach in example for Composite Z in Section 4.1) will be mixed together in liquid form. Solids will be separated from the resulting liquid composite to yield low water content (i.e., drip free) fine solids.

Or

b) Solids will be separated from liquid for each component of Composite 4 to yield low water content (i.e., drip free) fine solids for each component. Equal weights of the solids form of each component (following the approach in the example for Composite Z in Section 4.1) will be mixed together to yield Composite 4.

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TAB # 5

Replacement Pages for Daikin America, Inc. 1

¹Additional changes and corrections to the ECA document were identified after completion of the Public Review Process. EPA set in place a process whereby the needed changes(s) were made using strike-out with hand written correction(s) on each page (i.e., replacement page) of the ECA where such changes were needed. Each signatory was asked to acknowledge their concurrence by initialing and dating every change on each ECA replacement page. The ECA document contained under TAB # 1 contains the replacement pages originated by EPA. The pages under this Tab contain those replacement pages co-initialed by EPA and Daikin America, Inc.

Contains No Confidential Business Information

(D) Aqueous Fluoropolymer Dispersions Composite #4: (containing: Ethene, tetrafluoro-, polymer with trifluoro(pentafluoroethoxy)—ethene, CAS No. 31784-04-0; Ethene, tetrafluoro-, homopolymer, CAS No. 9002-84-0; 1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene), CAS No. 25067-11-2; Propane, 1,1,1,2,2,3,3-heptafluoro-3- [(trifluoroethenyl)oxy]-, polymer with tetrafluoroethene, CAS No. 26655-00-5; Ethene, tetrafluoro-, polymer with trifluoro(pentafluoroethexy)ethene; CAS No. 21784-04-0; 1-Propene, 1,1,2,3,3,3- hexafluoro-, polymer with 1,1-difluoroethene and tetrafluoroethene, CAS No. 25190-89-0; and polytetrafluoroethylene, DCN No. 6304000001803.

ST /19/105

The procedure for constructing each composite is described in Appendix A.4. The polymer components for each composite will be unfilled first quality product polymer, substantially free of inorganic constituents. Each component of the four composites to be tested under this ECA will be accompanied by a certificate of analysis showing it to meet applicable product specifications.

III. OBLIGATION OF SIGNATORY COMPANIES

- A. The Companies are bound by the terms of this ECA as specified below.
- B. Each Company shall be responsible for supplying the test substance(s) it manufactures for incorporation into the composite(s) to be tested under this ECA, as specified on each Company signature page and in Appendix A.3. The schedule for the testing program includes the deadline date by which the Companies must submit their contribution(s) to the facility(ies) that will be assembling the composites to be tested under this ECA. Any Company failing to comply with this ECA requirement will be in violation of this ECA as described in 40 CFR 790.65 (see Part XII of this ECA). In the event that one or more of the Companies are in violation as described above then the remaining Companies will inform EPA of the problem and request an EPA determination on how to proceed with the testing program described under this ECA. Each Company required to contribute to a particular composite is obligated to complete the testing required by this ECA for that composite. A Company shall not be responsible for any failure to perform its obligation under this ECA that is caused by circumstances beyond its control, that the Company could not have prevented through the exercise of due diligence.

⁸ EPA uses a variety of numerical identification systems for tracking chemicals. These include Chemical Abstract Service Registry numbers (CAS) (assigned to non-confidential listed chemicals), pre-manufacture notice (PMN) numbers (assigned by EPA when chemicals enter EPA's new chemical review process, document control numbers (DCN) (assigned by the Confidential Business Information Center for EPA tracking), and Accession (ACC) numbers (provided by EPA when a chemical identity requires protection as TSCA CBI). In addition, Polymer Exemption products will not have a TSCA Inventory ID number but may have a commercial trade identity.

Contains No Confidential Business Information

to seek judicial review of any rule that may be adopted by EPA that imposes requirements to test any of the fluoropolymer chemicals listed in Appendix A.1 to this ECA.

XXII. RESERVATION OF RIGHTS BY COMPANIES

By signing this ECA, the Companies are not admitting that the requirements of TSCA Section 4 have been satisfied for promulgating a test rule to generate the data required by this ECA.

The Companies contend that the documents generated for the incineration testing program under this ECA are protected from public disclosure under 5 U.S.C. section 552(b)(4) and 15 U.S.C. section 2613(a) and do not constitute studies subject to disclosure under 15 U.S.C. section 2613(b). Accordingly, the public information disclosure provisions of this ECA are, in the view of the Companies, a waiver of legal rights.

XXIII. IDENTITY OF THE COMPANIES AND PRINCIPAL TEST SPONSOR

The Principal Test Sponsor is:

Fluoropolymer Manufacturers Group Allen Weidman The Society of the Plastics Industry, Inc. 1801 K Streert, N.W., Suite 600K Washington, DC 20006 202-974-5233

The Companies subject to this ECA are:

AGC Chemicals Americas, Inc. 229 East 22nd Street, Bayonne, NJ 07002

Dyneon, LLC 6744 33rd Street, Oakdale, MN 55128

Daikin America, Inc. 20 Olympic Drive, Orangeburg, NY 10962 E.I. du Pont de Nemours and Company

Route 141 and Henry Clay / 1007 MARKET STREE

Wilmington, DE 19880-0711 / 1989

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Contains No Confidential Business Information

XXIV. SIGNATURE

TEST SPONSOR Dyneon, LLC 1, 2

Company technical contact person for handling correspondence marked as "Confidential"

Name:

George H. Millet

Title:

Director, Quality, Environment, Health and Safety

Address:

6744 33rd Street, Oakdale, MN 55128

Phone Number:

651-733-5637

	ECA S	ubject Chemicals f	or Dyneon, LLC *
Entry	Composite	CAS Registry#	CAS 9CI Name
1	Dry non-melt Fluoropolymer Resin	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer
2	Dry non-melt Fluoropolymer Resin	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- (trifluoroethenyl)oxy]-, polymer with tetrafluoroethene
3	Dry melt Fluoropolymer Resin	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene
4	Dry melt Fluoropolymer Resin	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- [(trifluoroethenyl)oxy]-, polymer with tetrafluoroethene
5	Dry melt Fluoropolymer Resin	CAS #25190-89-0	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with 1,1-difluoroethene and tetrafluoroethene
6	Dry melt Fluoropolymer Resin		

¹ Data in the table lists the chemical(s) and composite contributions for which Dyneon, LLC is responsible. The Company developed these data in response to EPA's letter of January 6, 2004. There is both a Public and CBI version of this page because the Company has asserted that data in this table are considered by them to be entitled to treatment as TSCA confidential business information (CBI) (see Part XIV. D. of this ECA regarding confidentiality of information).

² Dyneon, LLC is obligated under this ECA to perform Phase I PFOA Transport Testing (see Part III. C. and VII.A. of this ECA).

Entry	Composite	CAS Registry #	CAS 9CI Name
7	Dry melt Fluoropolymer Resin	CAS #35560-16-8	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with ethene and tetrafluoroethene
8	Dry non-melt Fluoroelastomer Gum	CAS #27029-05-6	1-Propene, polymer with tetrafluoroethene
9	Dry non-melt Fluoroelastomer Gum	CAS #54675-89-7	1-Propene, polymer with 1,1- difluoroethene and tetrafluoroethene
10	Dry non-melt Fluoroelastomer Gum	CAS #26425-79-6	Ethene, tetrafluoro-, polymer with trifluoro(trifluoromethoxy) ethene
11	Dry non-melt Fluoroelastomer Gum	CAS #9010-75-7	Ethene, chlorotrifluoro-, polymer with j, - difluoroethene
12	Dry non-melt Fluoroelastomer Gum	><	
13	Aqueous Dispersion	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer
14	Aqueous Dispersion	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene
15	Aqueous Dispersion	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- [(trifluoroethenyl)oxy]-, polymer with tetrafluoroethene
16	Aqueous Dispersion	CAS #25190-89-0	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with 1,1-difluoroethene and tetrafluoroethene

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Entries "X'd" out indicate redacted information claimed as CBI by the Company.

Contains No Confidential Business Information

XXIV. SIGNATURE

TEST SPONSOR

E.I. du Pont de Nemours and Company 1, 2

Company technical contact person for handling correspondence marked as "Confidential"

Name:

David W: Boothe

Title:

Strategic Planning Manager - DuPont Fluorosolutions

Address:

Route 141 & Henry Clay, Wilmington, DE 19880-0711 19805

Phone Number:

Chestrat Run 702

4417 Lancaster Pike

		wat Kan Co E				
	ECA Subject Chem	Subject Chemicals for E. I. du Pont de Nemours and Company				
Entry Composite CAS Registry #		CAS 9CI Name				
1	Dry non-melt Fluoropolymer Resin	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer			
2	Dry melt Fluoropolymer Resin	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene			
3	Dry melt Fluoropolymer Resin	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- (trifluoroethenyl)oxy]-, polymer with tetrafluoroethene			
4	Dry melt Fluoropolymer Resin	CAS #31784-04-0	Ethene, tetrafluoro-, polymer with trifluoro(pentafluoroethoxy)ethene			
5	Aqueous Dispersion	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer			
6	Aqueous Dispersion	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene			
7	Aqueous Dispersion	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- (trifluoroethenyl)oxy]-, polymer with tetrafluoroethene			

¹ Data in the table lists the chemical(s) and composite contributions for which E.I. du Pont de Nemours and Company is responsible. The Company developed these data in response to EPA's letter of January 6, 2004.

² E.I. du Pont de Nemours and Company is not obligated under this ECA to perform Phase I PFOA Transport Testing (see Part III. C. and VII.A. of this ECA).

APPENDIX A.3 COMPOSITION OF COMPOSITES TO BE TESTED

The four composite test substances for this test program are presented below in Table A.3-I with the fluoropolymer types, CAS numbers, and associated monomers for these fluoropolymers. Each fluoropolymer used in each relevant test substance composite will have been made using APFO.

Table A. 3-1. Test Substance Composites		TABB	
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Test Substance	Fluoropolymer Type		Associated Monomers
Composite 1 -	PTFE	9002-84-0	小食菜
ory non-melt resin	Modified PTFE	26655-00-5	TFE, PPVE
Composite 2 -	PEP	25067-11-2	TFE, HEP
Ory melt resins	PTA	26555-00-5 31784-04-0	TFE, PPVE TFE, PEVE
	THY	25190-89-0	TFE, HFP, VDE
•	STEE	68258-85-5	FFE, E
•	HTE	35560-16-8	TPE, NFP, E
Composite 3 - Yluoroelastomers	Fluoroelastomer Copolymers	9011-17-0	VDF, HFP
	Fluoroelastomer Terpolymers	25190-89-0	TEE, HEP, VDF
· ·	Base resistant elastomers	54675-89-7, 27029-05-6	TEE, P
	Perfluoroelastomers	Annual Control of the	TFE, PMVE
	CTPE alastomera	9010-75-7	CTFE, VFD
	Low temperature elastomers	CBI	IFE, VOF
cmposite 4 - queous	ets:	9002-84-0	TFR
ispersions	FEF	25067-11-2	TFE, HFP
· LE SETTE SE	PPA	26655-00-5 31784-04-0	TFE, PPVE
	THV	1	THE HERE
	TUX	たつてないよのおよれ	TPS, HEP, VDE

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Confidential business information (CBI) regarding the chemical identity of low temperature elastomers has been submitted to EPA under separate cover.

Contains No Confidential Business Information

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4.2.2 Composite 2

luf 10/6%.

FEP, PFA EEP, PEA, THV, ETEE, and HTE dry melt resins are available in powder form. Equal weights 19/20 of the powder form of each component (following the approach in the example for Composite Z in Section 4.1 above) will be mixed together in dry form to yield Composite 2.

4.2.3 Composite 3

Fluoroelastomers are available in slab, lump, or sheet form. Composite 3 will be prepared following one of the following approaches:

Equal weights of each component (following the approach in a) example for Composite Z in Section 4.1) will be mixed on a rubber mill to produce a homogenous slab of preset thickness to yield Composite 3.

Or

Each component of Composite 3 will be cyrogenically cooled (to b) make the elastomers brittle) and size-reduced (e.g., ground) to produce powder. Equal weights of the powder form of each component (following the approach in the example for Composite Z in Section 4.1) will be mixed together in dry form to yield Composite 3.

4.2.4 Composite 4

Aqueous dispersions of PTFE, FEP, PFA, and THV are available as dispersions containing 20 to 60% fluoropolymer solids by weight. Composite 4 will be prepared following one of the following approaches:

Equal weights (on a dry solids basis) of each component in a) aqueous dispersion form (following the approach in example for Composite Z in Section 4.1) will be mixed together in liquid form. Solids will be separated from the resulting liquid composite to yield low water content (i.e., drip free) fine solids.

Or

b) Solids will be separated from liquid for each component of Composite 4 to yield low water content (i.e., drip free) fine solids for each component. Equal weights of the solids form of each component (following the approach in the example for Composite Z in Section 4.1) will be mixed together to yield Composite 4.

TAB#6

Replacement Pages for Dyneon, LLC ¹

^{&#}x27;Additional changes and corrections to the ECA document were identified after completion of the Public Review Process. EPA set in place a process whereby the needed changes(s) were made using strike-out with hand written correction(s) on each page (i.e., replacement page) of the ECA where such changes were needed. Each signatory was asked to acknowledge their concurrence by initialing and dating every change on each ECA replacement page. The ECA document contained under TAB # 1 contains the replacement pages originated by EPA. The pages under this Tab contain those replacement pages co-initialed by EPA and Dyneon LLC.

Contains No Confidential Business Information

Aqueous Fluoropolymer Dispersions Composite #4: (containing:

Bthens, tetrafluoro-, polymer with trifluoro(pentafluoroethoxy)

ethens, CAS No. 31784-04-0; Ethens, tetrafluoro-, homopolymer,

CAS No. 9002-84-0; 1-Propens, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethens), CAS No. 25067-11-2; Propans,

1,1,1,2,3,3-heptafluoro-3- [(trifluoroethenyl)oxy]-, polymer with tetrafluoroethens, CAS No. 26655-00-5; Ethens, tetrafluoro-, polymer with trifluoro(pentafluoroethexy)ethens, CAS No.

31784-04-0; 1-Propens, 1,1,2,3,3,3- hexafluoro-, polymer with 1,1-difluoroethene and tetrafluoroethene, CAS No. 25190-89-0; and polytetrafluoroethylens, DCN No. 6304000001803.

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William Myon 1/13/05
William Myon 1/13/0

The procedure for constructing each composite is described in Appendix A.4. The polymer components for each composite will be unfilled first quality product polymer, substantially free of inorganic constituents. Each component of the four composites to be tested under this ECA will be accompanied by a certificate of analysis showing it to meet applicable product specifications.

III. OBLIGATION OF SIGNATORY COMPANIES

A. The Companies are bound by the terms of this ECA as specified below.

B. Each Company shall be responsible for supplying the test substance(s) it manufactures for incorporation into the composite(s) to be tested under this ECA, as specified on each Company signature page and in Appendix A.3. The schedule for the testing program includes the deadline date by which the Companies must submit their contribution(s) to the facility(ies) that will be assembling the composites to be tested under this ECA. Any Company failing to comply with this ECA requirement will be in violation of this ECA as described in 40 CFR 790.65 (see Part XII of this ECA). In the event that one or more of the Companies are in violation as described above then the remaining Companies will inform EPA of the problem and request an EPA determination on how to proceed with the testing program described under this ECA. Each Company required to contribute to a particular composite is obligated to complete the testing required by this ECA for that composite. A Company shall not be responsible for any failure to perform its obligation under this ECA that is caused by circumstances beyond its control, that the Company could not have prevented through the exercise of due diligence.

BPA uses a variety of numerical identification systems for tracking chemicals. These include Chemical Abstract Service Registry numbers (CAS) (assigned to non-confidential listed chemicals), pre-manufacture notice (PMN) numbers (assigned by EPA when chemicals enter EPA's new chemical review process, document control numbers (DCN) (assigned by the Confidential Business Information Center for EPA tracking), and Accession (ACC) numbers (provided by EPA when a chemical identity requires protection as TSCA CBI). In addition, Polymer Exemption products will not have a TSCA Inventory ID number but may have a commercial trade identity.

to seek judicial review of any rule that may be adopted by EPA that imposes requirements to test any of the fluoropolymer chemicals listed in Appendix A.1 to this ECA.

XXII. RESERVATION OF RIGHTS BY COMPANIES

By signing this ECA, the Companies are not admitting that the requirements of TSCA Section 4 have been satisfied for promulgating a test rule to generate the data required by this ECA.

The Companies contend that the documents generated for the incineration testing program under this ECA are protected from public disclosure under 5 U.S.C. section 552(b)(4) and 15 U.S.C. section 2613(a) and do not constitute studies subject to disclosure under 15 U.S.C. section 2613(b). Accordingly, the public information disclosure provisions of this ECA are, in the view of the Companies, a waiver of legal rights.

XXIII. IDENTITY OF THE COMPANIES AND PRINCIPAL TEST SPONSOR

The Principal Test Sponsor is:

Fluoropolymer Manufacturers Group Allen Weidman The Society of the Plastics Industry, Inc. 1801 K Streert, N.W., Suite 600K Washington, DC 20006 202-974-5233

The Companies subject to this ECA are:

AGC Chemicals Americas, Inc. 229 East 22nd Street, Bayonne, NJ 07002

Daikin America, Inc. 20 Olympic Drive, Orangeburg, NY 10962 Dyneon, LLC 6744 33rd Street, Oakdale, MN 55128

E.I. du Pont de Nemours and Company

Route 141 and Henry Clay /007 MARVET STRE

Wilmington, DE 19880-0711 /9898

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Contains No Confidential Business Information

XXIV. SIGNATURE

TEST SPONSOR Dyneon, LLC 1, 2

Company technical contact person for handling correspondence marked as "Confidential"

Name:

George H. Millet

Title:

Director, Quality, Environment, Health and Safety

Address:

6744 33rd Street, Oakdale, MN 55128

Phone Number:

651-733-5637

	ECA Subject Chemicals for Dyneon, LLC *				
Entry	Composite	Composite CAS Registry # CAS 9CI Name			
1	Dry non-melt Fluoropolymer Resin	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer		
2	Dry non-melt Fluoropolymer Resin	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- (trifluoroethenyl)oxy]-, polymer with tetrafluoroethene		
3	Dry melt Fluoropolymer Resin	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene		
. 4	Dry melt Fluoropolymer Resin	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- [(trifluoroethenyl)oxy]-, polymer with tetrafluoroethene		
5	Dry melt Fluoropolymer Resin	CAS #25190-89-0	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with 1,1-difluoroethene and tetrafluoroethene		
6	Dry melt Fluoropolymer Resin	><			

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Data in the table lists the chemical(s) and composite contributions for which Dyneon, LLC is responsible. The Company developed these data in response to EPA's letter of January 6, 2004. There is both a Public and CBI version of this page because the Company has asserted that data in this table are considered by them to be entitled to treatment as TSCA confidential business information (CBI) (see Part XIV. D. of this ECA regarding confidentiality of information).

² Dyneon, LLC is obligated under this ECA to perform Phase I PFOA Transport Testing (see Part III. C. and VII.A. of this ECA).

Entry	Composite	CAS Registry #	CAS 9CI Name	
7	Dry melt Fluoropolymer Resin	CAS #35560-16-8	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with ethene and tetrafluoroethene	
8	Dry non-melt Fluoroelastomer Gum	CAS #27029-05-6	1-Propene, polymer with tetrafluoroethene	
9	Dry non-melt Fluoroelastomer Gum	CAS #54675-89-7	1-Propene, polymer with 1,1- difluoroethene and tetrafluoroethene	
10	Dry non-melt Fluoroelastomer Gum	CAS #26425-79-6	Ethene, tetrafluoro-, polymer with trifluoro(trifluoromethoxy) ethene	
11	Dry non-melt Fluoroelastomer Gum	CAS #9010-75-7	Ethene, chlorotrifluoro-, polymer with Ji-difluoroethene	
12	Dry non-melt Fluoroelastomer Gum			
13	Aqueous Dispersion	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer	
14	Aqueous Dispersion	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene	
15	Aqueous Dispersion	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- [(trifluoroethenyl)oxy]-, polymer with tetrafluoroethene	
16	Aqueous Dispersion	CAS #25190-89-0	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with 1,1-difluoroethene and tetrafluoroethene	

XXIV. SIGNATURE

TEST SPONSOR

E.I. du Pont de Nemours and Company 1, 2

Company technical contact person for handling correspondence marked as "Confidential"

Name:

David W. Boothe

Title:

Address:

Strategic Planning Manager - DuPont Fluorosolutions Route 141 & Henry Clay, Wilmington, DE 19880-0711 19805

Phone Number:

Chestnat Run 702 4417 Lancaster Pike

	ECA Subject Chemicals for E. I. du Pont de Nemours and Company				
Entry	Composite	CAS Registry #	CAS 9CI Name		
1	Dry non-melt Fluoropolymer Resin	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer		
2	Dry melt Fluoropolymer Resin	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene		
3	Dry melt Fluoropolymer Resin	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- (trifluoroethenyl)oxy]-, polymer with tetrafluoroethene		
4	Dry melt Fluoropolymer Resin	CAS #31784-04-0	Ethene, tetrafluoro-, polymer with trifluoro(pentafluoroethoxy)ethene		
5	Aqueous Dispersion	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer		
6	Aqueous Dispersion	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene		
7	Aqueous Dispersion	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- (trifluoroethenyl)oxy]-, polymer with tetrafluoroethene		

¹ Data in the table lists the chemical(s) and composite contributions for which E.I. du Pont de Nemours and Company is responsible. The Company developed these data in response to EPA's letter of January 6, 2004.

² E.I. du Pont de Nemours and Company is not obligated under this ECA to perform Phase I PFOA Transport Testing (see Part III. C. and VII.A. of this ECA).

APPENDIX A.3 COMPOSITION OF COMPOSITES TO BE TESTED

The four composite test substances for this test program are presented below in Table A.3-1 with the fluoropolymer types, CAS numbers, and associated monomers for these fluoropolymers. Each fluoropolymer used in each relevant test substance composite will have been made using APFO.

Table A.3-1. Test Substance Composites by Type

Test Substance	Fluoropolymer Type		a	ociato Mors	sd.
Composite 1 -	PTFE	9002-84-0	TEE		
Dry non-melt resin	Modified PIFE	26653-00-5	TEE,	PPVE	
Composite 2 -	PBP	25067-11-2	TFE,	HEP	
Dry melt resins	PFA	26655-00-5 31784-04-0	3 . ×	PEVE	
	THY	25190-89-0		HFP,	ć
	etee Hie	68258-85-5 35560-16-8	TFE,	E HFP,	E
Composite 3 - Fluoroelastomers	Fluoroelastomer	9011-17-0	VDF,		
	Fluoroelastomer Terpolymers	25190-89-0	TTE,	RFP,	VDF
	Base resistant elastomers	54675-89-7, 27029-05-6	TFE.	-	P
	Perfluoroelastomers		TFE,	PMVE	
•	CTFE elastomers	9010-75-7	CTFE,		
	Low temperature elastomers	CBI	TFE,	VOE	
composite 4 - Aqueous	PTFS	9002-84-0	TFE		
ispersions	fep .	25067-11-2	TFE,	HFP	
. • • • • • • • • • • • • • • • • • • •	PFA	26655-00-5 31784-04-8	TEE,	PPVE	
	CHV	25190-89-D	 	HFP,	VDE

William Myers 10/11/04

Confidential business information (CBI) regarding the chemical identity of low temperature elastomers has been submitted to EPA under separate cover.

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4.2.2 Composite 2

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FEP, PFA ETFÉ

EEP, PEA, THV, ETEE, and HTE dry melt resins are available in powder form. Equal weights of the powder form of each component (following the approach in the example for Composite Z in Section 4.1 above) will be mixed together in dry form to yield Composite 2.

4.2.3 Composite 3

Fluoroelastomers are available in slab, lump, or sheet form. Composite 3 will be prepared following one of the following approaches:

a) Equal weights of each component (following the approach in example for Composite Z in Section 4.1) will be mixed on a rubber mill to produce a homogenous slab of preset thickness to yield Composite 3.

Or

b) Each component of Composite 3 will be cyrogenically cooled (to make the elastomers brittle) and size-reduced (e.g., ground) to produce powder. Equal weights of the powder form of each component (following the approach in the example for Composite Z in Section 4.1) will be mixed together in dry form to yield Composite 3.

4.2.4 Composite 4

Aqueous dispersions of PTFE, FEP, PFA, and THV are available as dispersions containing 20 to 60% fluoropolymer solids by weight. Composite 4 will be prepared following one of the following approaches:

a) Equal weights (on a dry solids basis) of each component in aqueous dispersion form (following the approach in example for Composite Z in Section 4.1) will be mixed together in liquid form. Solids will be separated from the resulting liquid composite to yield low water content (i.e., drip free) fine solids.

Or

b) Solids will be separated from liquid for each component of Composite 4 to yield low water content (i.e., drip free) fine solids for each component. Equal weights of the solids form of each component (following the approach in the example for Composite Z in Section 4.1) will be mixed together to yield Composite 4.

TAB # 7

Replacement Pages for E.I du Pont de Nemours and Company

Additional changes and corrections to the ECA document were identified after completion of the Public Review Process. EPA set in place a process whereby the needed changes(s) were made using strike-out with hand written correction(s) on each page (i.e., replacement page) of the ECA where such changes were needed. Each signatory was asked to acknowledge their concurrence by initialing and dating every change on each ECA replacement page. The ECA document contained under TAB # 1 contains the replacement pages originated by EPA. The pages under this Tab contain those replacement pages co-initialed by EPA and E.I du Pont de Nemours and Company.

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sions Composite #4: (containing:

with trifluoro(pentafluoroethoxy)

Ethene, tetrafluoro-, homopolymer,

1,1,2,3,3,3-hexafluoro-, polymer

10. 25067-11-2; Propane,

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(D) Aqueous Fluoropolymer Dispersions Composite #4: (containing: Ethene, tetrafluoro-, polymer with trifluoro(pentafluoroethoxy)—ethene, CAS No. 31784-04-0; Ethene, tetrafluoro-, homopolymer, CAS No. 9002-84-0; 1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene), CAS No. 25067-11-2; Propane, 1,1,1,2,2,3,3-heptafluoro-3- [(trifluoroethenyl)oxy]-, polymer with tetrafluoroethene, CAS No. 26655-00-5; Ethene, tetrafluoro-, polymer with trifluoro(pentafluoroethoxy)ethene, CAS No. 25190-89-0; and polytetrafluoroethylene, DCN No. 63040000018Q).*

The procedure for constructing each composite is described in Appendix A.4. The polymer components for each composite will be unfilled first quality product polymer, substantially free of inorganic constituents. Each component of the four composites to be tested under this ECA will be accompanied by a certificate of analysis showing it to meet applicable product specifications.

III. OBLIGATION OF SIGNATORY COMPANIES

- A. The Companies are bound by the terms of this ECA as specified below.
- B. Each Company shall be responsible for supplying the test substance(s) it manufactures for incorporation into the composite(s) to be tested under this ECA, as specified on each Company signature page and in Appendix A.3. The schedule for the testing program includes the deadline date by which the Companies must submit their contribution(s) to the facility(ies) that will be assembling the composites to be tested under this ECA. Any Company failing to comply with this ECA requirement will be in violation of this ECA as described in 40 CFR 790.65 (see Part XII of this ECA). In the event that one or more of the Companies are in violation as described above then the remaining Companies will inform EPA of the problem and request an EPA determination on how to proceed with the testing program described under this ECA. Each Company required to contribute to a particular composite is obligated to complete the testing required by this ECA for that composite. A Company shall not be responsible for any failure to perform its obligation under this ECA that is caused by circumstances beyond its control, that the Company could not have prevented through the exercise of due diligence.

EPA uses a variety of numerical identification systems for tracking chemicals. These include Chemical Abstract Service Registry numbers (CAS) (assigned to non-confidential listed chemicals), pre-manufacture notice (PMN) numbers (assigned by EPA when chemicals enter EPA's new chemical review process, document control numbers (DCN) (assigned by the Confidential Business Information Center for EPA tracking), and Accession (ACC) numbers (provided by EPA when a chemical identity requires protection as TSCA CBI). In addition, Polymer Exemption products will not have a TSCA Inventory ID number but may have a commercial trade identity.

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to seek judicial review of any rule that may be adopted by EPA that imposes requirements to test any of the fluoropolymer chemicals listed in Appendix A.1 to this ECA.

XXII. RESERVATION OF RIGHTS BY COMPANIES

By signing this ECA, the Companies are not admitting that the requirements of TSCA Section 4 have been satisfied for promulgating a test rule to generate the data required by this ECA.

The Companies contend that the documents generated for the incineration testing program under this ECA are protected from public disclosure under 5 U.S.C. section 552(b)(4) and 15 U.S.C. section 2613(a) and do not constitute studies subject to disclosure under 15 U.S.C. section 2613(b). Accordingly, the public information disclosure provisions of this ECA are, in the view of the Companies, a waiver of legal rights.

XXIII. IDENTITY OF THE COMPANIES AND PRINCIPAL TEST SPONSOR

The Principal Test Sponsor is:

Fluoropolymer Manufacturers Group Allen Weidman The Society of the Plastics Industry, Inc. 1801 K Streert, N.W., Suite 600K Washington, DC 20006 202-974-5233

The Companies subject to this ECA are:

AGC Chemicals Americas, Inc. 229 East 22nd Street, Bayonne, NJ 07002

Daikin America, Inc. 20 Olympic Drive, Orangeburg, NY 10962 Dyneon, LLC 6744 33rd Street, Oakdale, MN 55128

E.I. du Pont de Nemours and Company

- Route 141 and Henry Clay - 1007 MARVET STREI

Wilmington, DE 19880-0711 - 19898

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XXIV. SIGNATURE

TEST SPONSOR Dyneon, LLC 1, 2

Company technical contact person for handling correspondence marked as "Confidential"

Name:

George H. Millet

Title:

Director, Quality, Environment, Health and Safety

Address:

6744 33rd Street, Oakdale, MN 55128

Phone Number:

651-733-5637

	ECA Subject Chemicals for Dyneon, LLC *				
Entry	Composite	CAS Registry #	CAS 9CI Name		
1	Dry non-melt Fluoropolymer Resin	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer		
2	Dry non-melt Fluoropolymer Resin	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- (trifluoroethenyl)oxy]-, polymer with tetrafluoroethene		
3	Dry melt Fluoropolymer Resin	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene		
4	Dry melt Fluoropolymer Resin	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- [(trifluoroethenyl)oxy]-, polymer with tetrafluoroethene		
5	Dry melt Fluoropolymer Resin	CAS #25190-89-0	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with 1,1-difluoroethene and tetrafluoroethene		
6	Dry melt Fluoropolymer Resin	><			

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Data in the table lists the chemical(s) and composite contributions for which Dyneon, LLC is responsible. The Company developed these data in response to EPA's letter of January 6, 2004. There is both a Public and CBI version of this page because the Company has asserted that data in this table are considered by them to be entitled to treatment as TSCA confidential business information (CBI) (see Part XIV. D. of this ECA regarding confidentiality of information).

² Dyneon, LLC is obligated under this ECA to perform Phase I PFOA Transport Testing (see Part III. C. and VII.A. of this ECA).

Entry	Composite	CAS Registry #	CAS 9CI Name	
7	Dry melt Fluoropolymer Resin	CAS #35560-16-8	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with ethene and tetrafluoroethe	
8	Dry non-melt Fluoroelastomer Gum	CAS #27029-05-6	1-Propene, polymer with tetrafluoroethe	
9	Dry non-melt Fluoroelastomer Gum	CAS #54675-89-7	1-Propene, polymer with 1,1- difluoroethene and tetrafluoroethene	
10	Dry non-melt Fluoroelastomer Gum	CAS #26425-79-6	Ethene, tetrafluoro-, polymer with trifluoro(trifluoromethoxy) ethene	
11	Dry non-melt Fluoroelastomer Gum	CAS #9010-75-7	Ethene, chlorotrifluoro-, polymer with J difluoroethene	
12	Dry non-melt Fluoroelastomer Gum			
13	Aqueous Dispersion	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer	
14	Aqueous Dispersion	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene	
15	Aqueous Dispersion	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- [trifluoroethenyl)oxy]-, polymer with tetrafluoroethene	
16	Aqueous Dispersion	CAS #25190-89-0	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with 1,1-difluoroethene and tetrafluoroethene	

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XXIV. SIGNATURE

TEST SPONSOR

E.I. du Pont de Nemours and Company 1, 2

Company technical contact person for handling correspondence marked as "Confidential"

Name:

David W. Boothe

Title:

David W. Boothe

Strategic Planning Manager - DuPont Fluorosolutions -

Address:

Route 141 & Henry Clay, Wilmington, DE 19880-0711 1980S

Phone Number:

4417 Lancaster Pike

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	ECA Subject Chemicals for E. I. du Pont de Nemours and Company					
Entry	Composite	CAS Registry #	CAS 9CI Name			
1	Dry non-melt Fluoropolymer Resin	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer			
2	Dry melt Fluoropolymer Resin	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene			
3	Dry melt Fluoropolymer Resin	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- (trifluoroethenyl)oxy]-, polymer with tetrafluoroethene			
4	Dry melt Fluoropolymer Resin	CAS #31784-04-0	Ethene, tetrafluoro-, polymer with trifluoro(pentafluoroethoxy)ethene			
5	Aqueous Dispersion	CAS #9002-84-0	Ethene, tetrafluoro-, homopolymer			
6	Aqueous Dispersion	CAS #25067-11-2	1-Propene, 1,1,2,3,3,3-hexafluoro-, polymer with tetrafluoroethene			
7	Aqueous Dispersion	CAS #26655-00-5	Propane, 1,1,1,2,2,3,3-heptafluoro-3- (trifluoroethenyl)oxy]-, polymer with tetrafluoroethene			

¹ Data in the table lists the chemical(s) and composite contributions for which E.I. du Pont de Nemours and Company is responsible. The Company developed these data in response to EPA's letter of January 6, 2004.

² E.I. du Pont de Nemours and Company is not obligated under this ECA to perform Phase I PFOA Transport Testing (see Part III. C. and VII.A. of this ECA).

APPENDIX A.3 COMPOSITION OF COMPOSITES TO BE TESTED

The four composite test substances for this test program are presented below in Table A.3-1 with the fluoropolymer types, CAS numbers, and associated monomers for these fluoropolymers. Each fluoropolymer used in each relevant test substance composite will have been made using APFO.

Table A.3-1. Test Substance Composites by Type

Test Substance	Fluoropolymer Type		Associated Monomers
Composite 1 -	PTFS	9002-84-0	ales.
Dry noo-welt resin	Modified FIFE	26655-00-5	TFE, PPVE
Composite 2 -	erp	25067-11-2	TFE, HEP
Dry melt resins	eva	26655-00-5	TFE, PPVE
•		31784-04-0	TFE, PEVE
	THY	25190-89-0	FFR, HFP, VDF
•	ETEE	60258-05-5	TFE, E
• •	HTE	35560-16-8	TFE, HCP, B
Composite 3 -	Fluoroelastomer	9011-17-0	VDP, HPP
Fluoroelastomers	Copolymers	•	
• • •	Fluoroelastomer	25190-89-0	TTE, RFP, VDF
•	Terpolymera		
	Base resistant		TFE, VDF, P
	elastomers	27029-05-6	TEE, P
	Perfluoroelastomers	26425-79-6	TFE, PMVE
	CTFE elastomers	9010-75-7	CIFE, VED
	Low temperature	,	TPE, VOE
	elastomers	CBI	
Composite 4 -	PTES	9002-84-0	TP2
Aqueous			
)ispersions	rep	25067-11-2	ree, hpp
	PFA	26655-00-5	FFE, PPVE
		31704-04-0	TRE, PEVE
	THV		CFE, HEP, VOF

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Confidential business information (CBI) regarding the chemical identity of low temperature elastomers has been submitted to EPA under separate cover.

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4.2.2 Composite 2

EEP, PEA, THV, ETEE, and HTE dry melt resins are available in powder form. Equal weights of the powder form of each component (following the approach in the in Section 4.1 above) will be mixed together in dry form to yield Composite 2.

4.2.3 Composite 3

Fluoroelastomers are available in slab, lump, or sheet form. Composite 3 will be prepared following one of the following approaches:

Equal weights of each component (following the approach in a) example for Composite Z in Section 4.1) will be mixed on a rubber mill to produce a homogenous slab of preset thickness to yield Composite 3.

Or

Each component of Composite 3 will be cyrogenically cooled (to **b**) make the elastomers brittle) and size-reduced (e.g., ground) to produce powder. Equal weights of the powder form of each component (following the approach in the example for Composite Z in Section 4.1) will be mixed together in dry form to yield Composite 3.

4.2.4 Composite 4

Aqueous dispersions of PTFE, FEP, PFA, and THV are available as dispersions containing 20 to 60% fluoropolymer solids by weight. Composite 4 will be prepared following one of the following approaches:

a) Equal weights (on a dry solids basis) of each component in aqueous dispersion form (following the approach in example for Composite Z in Section 4.1) will be mixed together in liquid form. Solids will be separated from the resulting liquid composite to yield low water content (i.e., drip free) fine solids.

Or

b) Solids will be separated from liquid for each component of Composite 4 to yield low water content (i.e., drip free) fine solids for each component. Equal weights of the solids form of each component (following the approach in the example for Composite Z in Section 4.1) will be mixed together to yield Composite 4.